

**Reference****Differential Form****Integral Form****Gauss's law**

$$\nabla \cdot \mathbf{D} = \rho_v$$

$$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$$

**Faraday's law**

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s}$$

**No magnetic charges**

$$\nabla \cdot \mathbf{B} = 0$$

$$\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$$

**(Gauss's law for magnetism)****Ampère's law**

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$

$$\oint_C \mathbf{H} \cdot d\mathbf{l} = \int_S \left( \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{s}$$



# Statics

## stat-ic

adj.

1. **a.** Having no motion; being at rest; quiescent.  
**b.** Fixed; stationary.
2. *Physics* Of or relating to bodies at rest or forces that balance each other.
3. *Electricity* Of, relating to, or producing stationary charges; electrostatic.
4. Of, relating to, or produced by random radio noise.
- n.*
1. Random noise, such as crackling in a receiver or specks on a television screen, produced by atmospheric disturbance of the signal.
2. *Informal*
- a.** Back talk.
- b.** Interference; obstruction.
- c.** Angry or heated criticism.

For the special case of **no** time variations (i.e. *statics*) the electric and magnetic fields are de-coupled, and we can treat them separately!

$$\nabla \cdot \mathbf{D} = \rho_v$$

$$\nabla \times \mathbf{E} = -\cancel{\frac{\partial \mathbf{B}}{\partial t}} = 0$$

Electrostatics

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \cancel{\frac{\partial \mathbf{D}}{\partial t}} = \mathbf{J}$$

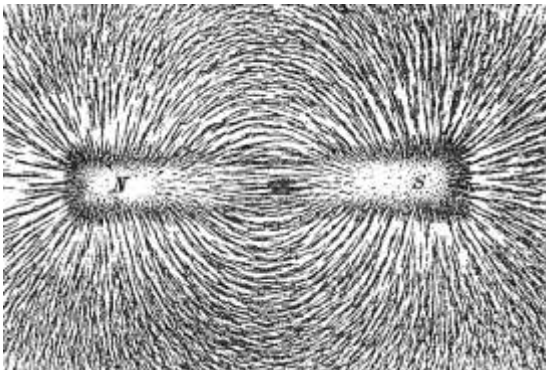
Magnetostatics

Stationary Charge

→ (static) Electric Fields

Constant Current (e.g. moving charge)

→ (static) magnetic Field



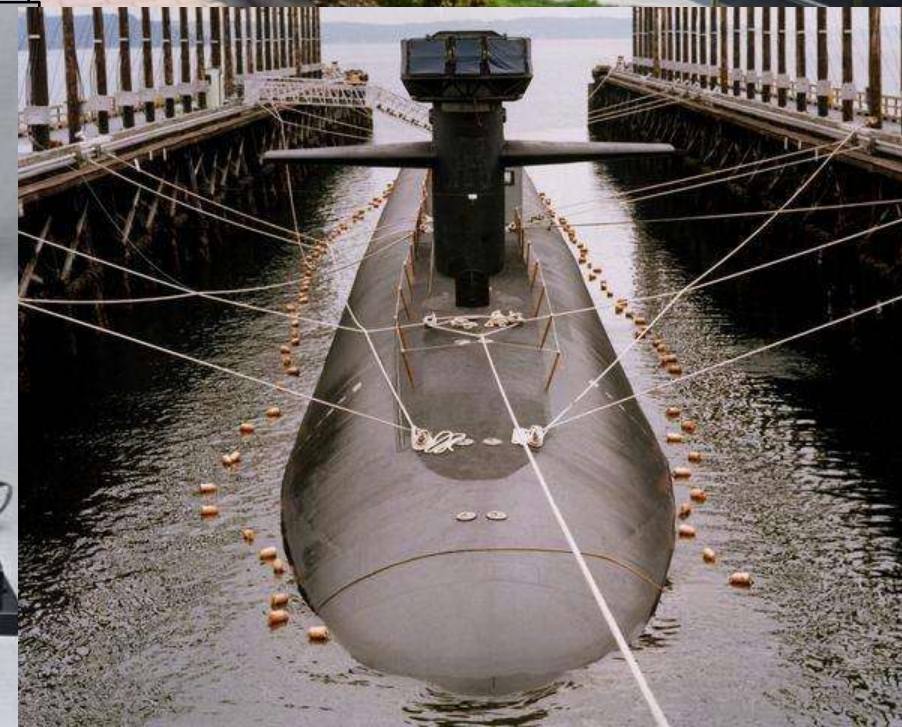
where  $\vec{B} = \mu \vec{H}$

magnetic  
Flux density

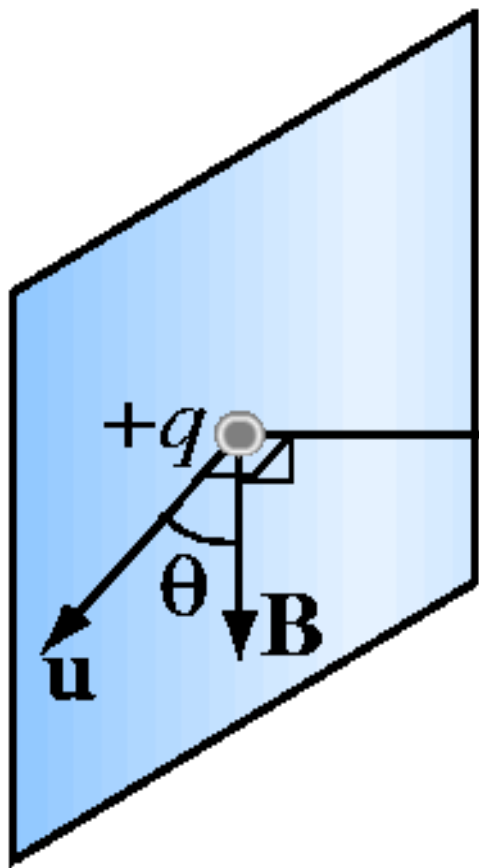
Magnetic Field  
Intensity

magnetic permeability

# Magnetostatics







Lorentz:

$$\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$$

$$\mathbf{F}_m = quB \sin \theta$$



Magnetic component of force

How we define our fields!

**Exercise 5.1** An electron moving in the positive  $x$ -direction perpendicular to a magnetic field experiences a deflection in the negative  $z$ -direction. What is the direction of the magnetic field?

$$q = -e$$

$$\mathbf{u} = \hat{x}u$$

$$\mathbf{F}_m = -\hat{z}F_m$$

$$-\hat{z}F_m = -\hat{x}ue \times \mathbf{B}$$

For the cross product to apply,  $\mathbf{B}$  has to be in the positive  $y$ -direction.

# Magnetic Force on a Current Element

$$\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$$

Differential force  $d\mathbf{F}_m$  on a differential current  $I d\mathbf{l}$ :

$$d\mathbf{F}_m = I d\mathbf{l} \times \mathbf{B} \quad (\text{N}), \quad (5.9)$$

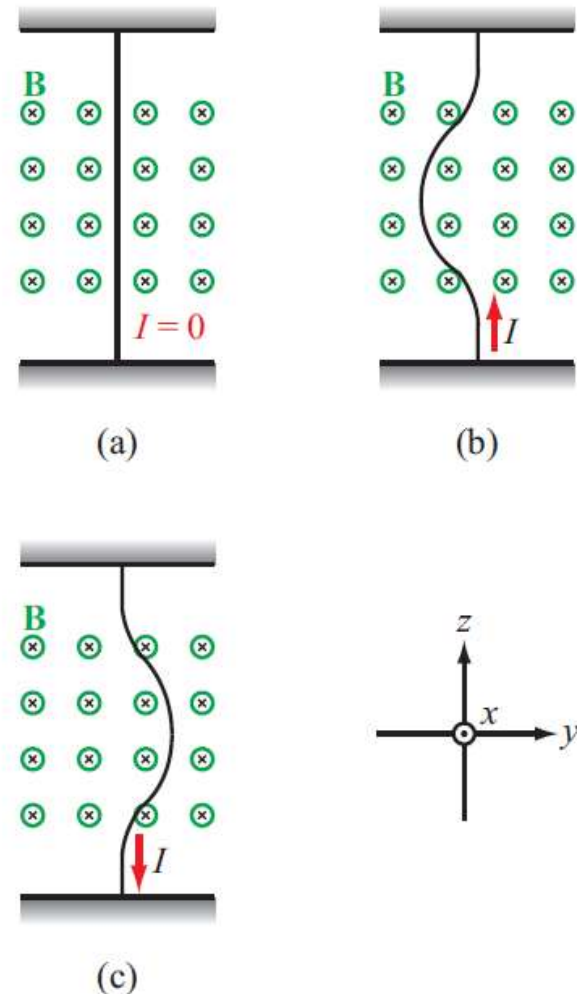
For a closed circuit of contour  $C$  carrying a current  $I$ , the total magnetic force is

$$\mathbf{F}_m = I \oint_C d\mathbf{l} \times \mathbf{B} \quad (\text{N}), \quad (5.10)$$

If the closed wire shown in Fig. 5-3(a) resides in a uniform external magnetic field  $\mathbf{B}$ , then  $\mathbf{B}$  can be taken outside the integral in Eq. (5.10), in which case

$$\mathbf{F}_m = I \left( \oint_C d\mathbf{l} \right) \times \mathbf{B} = 0. \quad (5.11)$$

*This result, which is a consequence of the fact that the vector sum of the infinitesimal vectors  $d\mathbf{l}$  over a closed path equals zero, states that the total magnetic force on any closed current loop in a uniform magnetic field is zero.*



**Figure 5-2:** When a slightly flexible vertical wire is placed in a magnetic field directed into the page (as denoted by the crosses), it is (a) not deflected when the current through it is zero, (b) deflected to the left when  $I$  is upward, and (c) deflected to the right when  $I$  is downward.

# Magnetic Torque on Current Loop

$$\mathbf{T} = \mathbf{d} \times \mathbf{F} \quad (\text{N}\cdot\text{m})$$

$$\mathbf{F}_1 = I(-\hat{y}b) \times (\hat{x}B_0) = \hat{z}IbB_0,$$

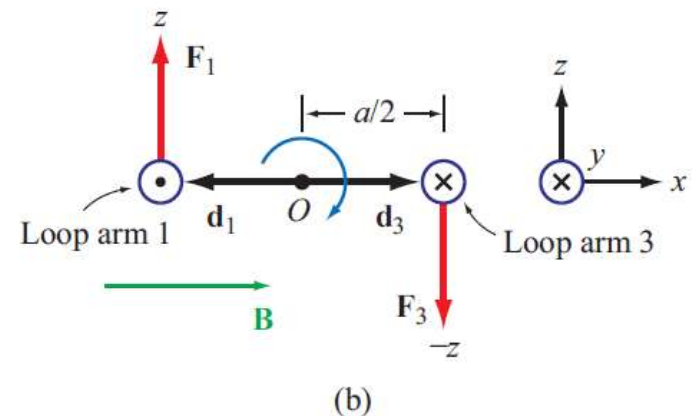
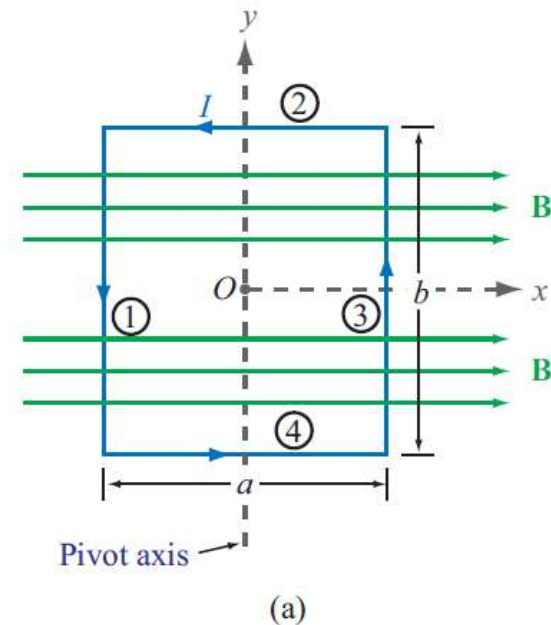
$$\mathbf{F}_3 = I(\hat{y}b) \times (\hat{x}B_0) = -\hat{z}IbB_0.$$

No forces on arms 2 and 4 ( because  $I$  and  $B$  are parallel, or anti-parallel)

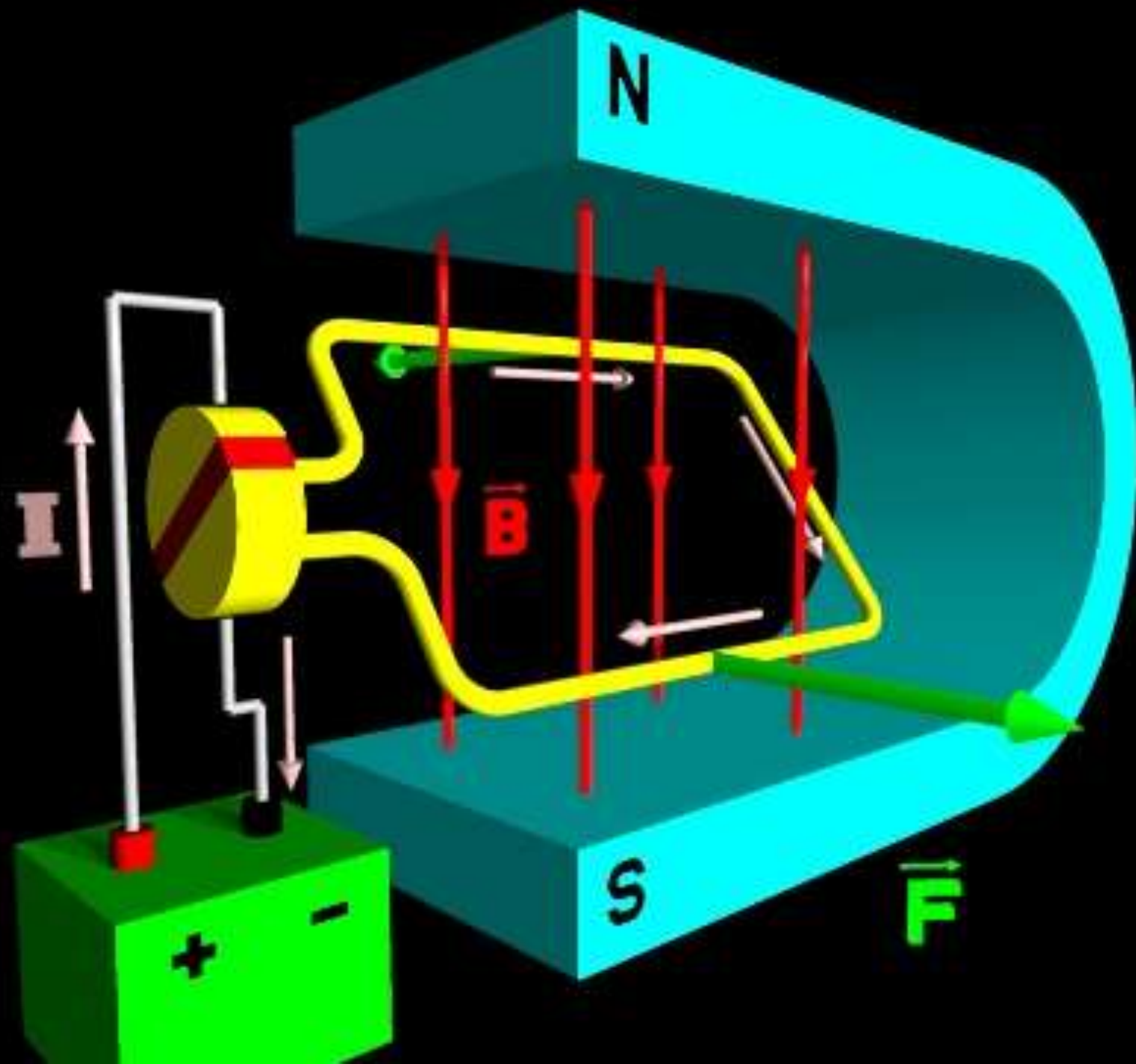
Magnetic torque:

$$\begin{aligned} \mathbf{T} &= \mathbf{d}_1 \times \mathbf{F}_1 + \mathbf{d}_3 \times \mathbf{F}_3 \\ &= \left(-\hat{x} \frac{a}{2}\right) \times (\hat{z}IbB_0) + \left(\hat{x} \frac{a}{2}\right) \times (-\hat{z}IbB_0) \\ &= \hat{y}IabB_0 = \hat{y}IA B_0, \end{aligned}$$

Area of Loop



**Figure 5-6:** Rectangular loop pivoted along the y-axis: (a) front view and (b) bottom view. The combination of forces  $\mathbf{F}_1$  and  $\mathbf{F}_3$  on the loop generates a torque that tends to rotate the loop in a clockwise direction as shown in (b).

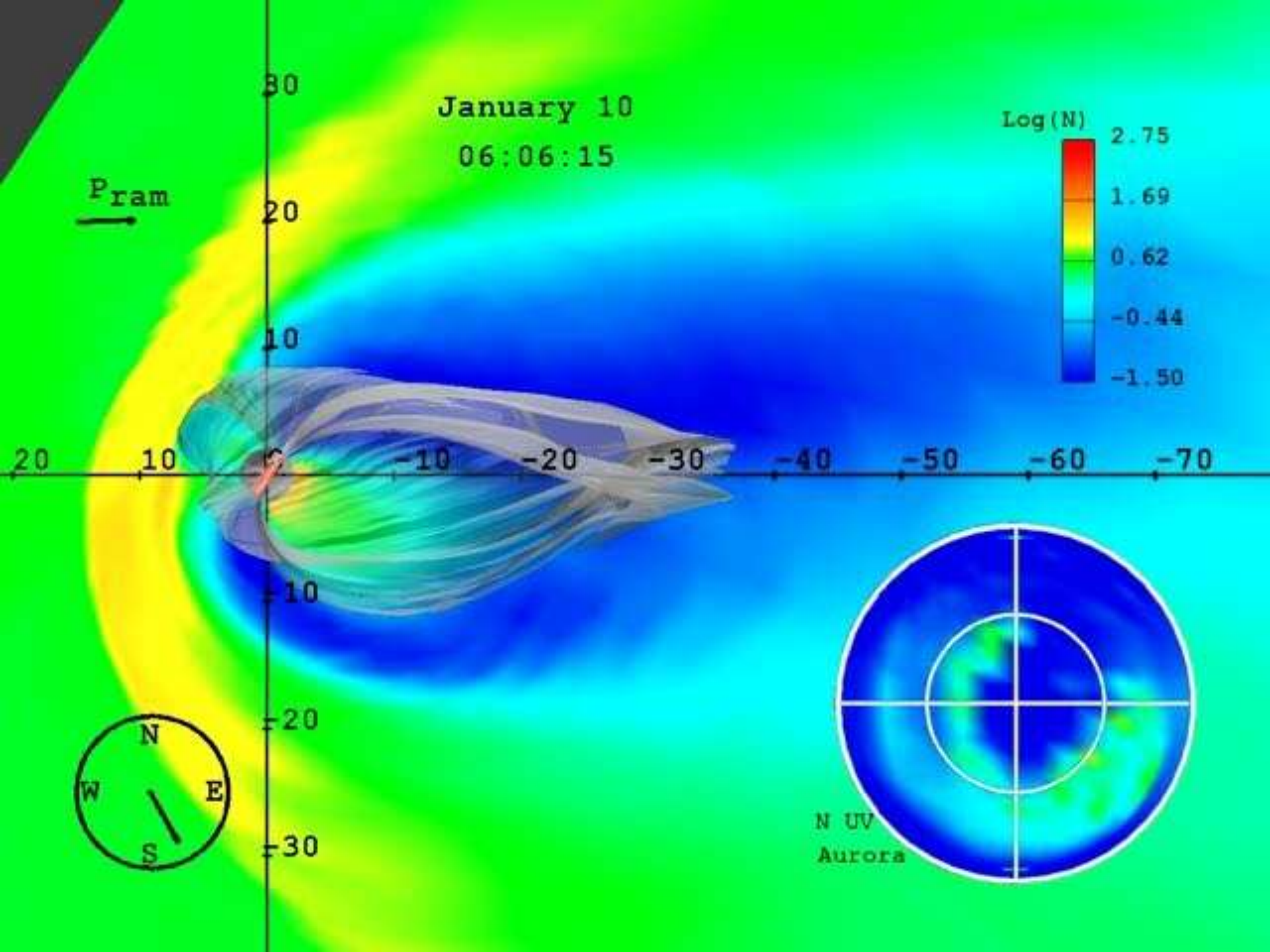


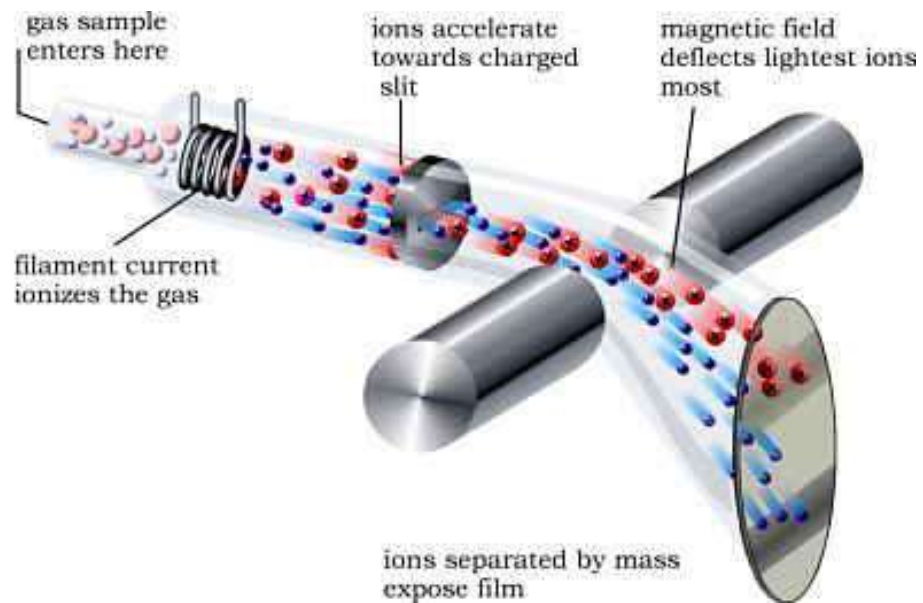
# Electric vs Magnetic Comparison

**Table 5-1:** Attributes of electrostatics and magnetostatics.

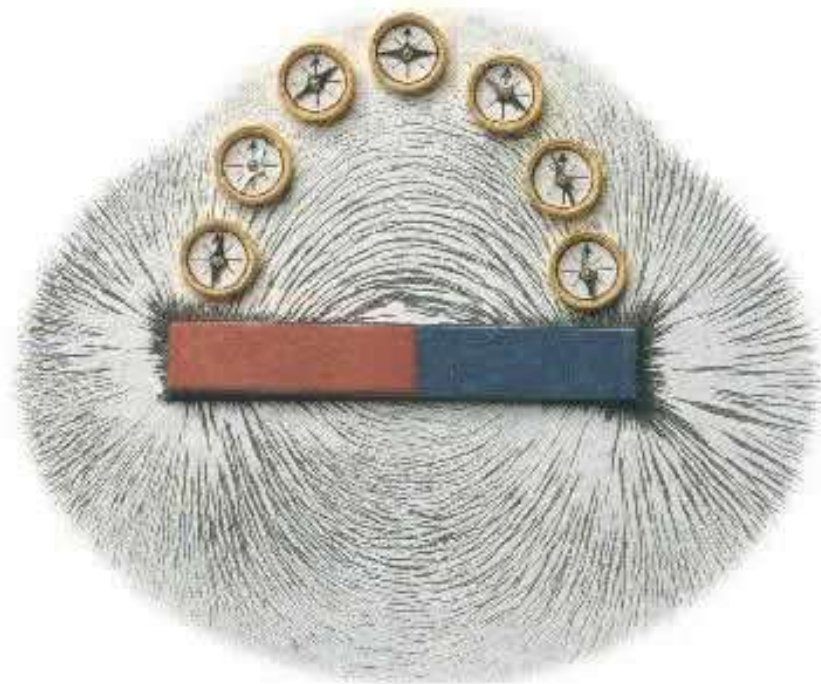
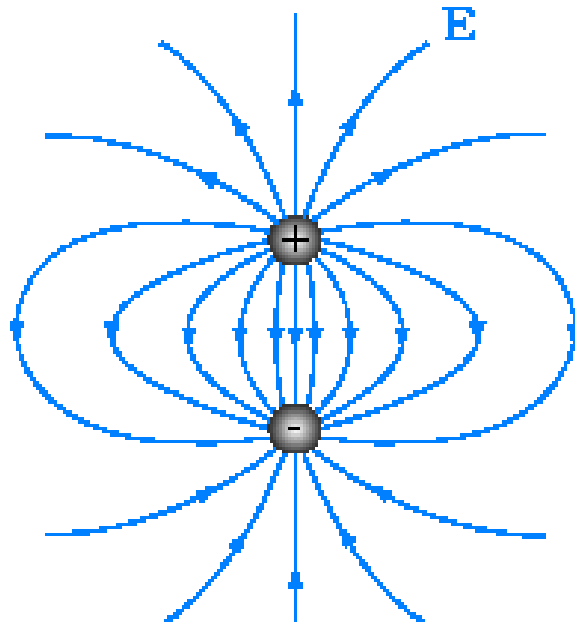
Attribute	Electrostatics	Magnetostatics
<b>Sources</b>	Stationary charges $\rho_v$	Steady currents $\mathbf{J}$
<b>Fields and Fluxes</b>	$\mathbf{E}$ and $\mathbf{D}$	$\mathbf{H}$ and $\mathbf{B}$
<b>Constitutive parameter(s)</b>	$\epsilon$ and $\sigma$	$\mu$
<b>Governing equations</b>		
• <b>Differential form</b>	$\nabla \cdot \mathbf{D} = \rho_v$ $\nabla \times \mathbf{E} = 0$	$\nabla \cdot \mathbf{B} = 0$ $\nabla \times \mathbf{H} = \mathbf{J}$
• <b>Integral form</b>	$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$ $\oint_C \mathbf{E} \cdot d\mathbf{l} = 0$	$\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$ $\oint_C \mathbf{H} \cdot d\mathbf{l} = I$
<b>Potential</b>	Scalar $V$ , with $\mathbf{E} = -\nabla V$	Vector $\mathbf{A}$ , with $\mathbf{B} = \nabla \times \mathbf{A}$
<b>Energy density</b>	$w_e = \frac{1}{2} \epsilon E^2$	$w_m = \frac{1}{2} \mu H^2$
<b>Force on charge <math>q</math></b>	$\mathbf{F}_e = q\mathbf{E}$	$\mathbf{F}_m = q\mathbf{u} \times \mathbf{B}$
<b>Circuit element(s)</b>	$C$ and $R$	$L$



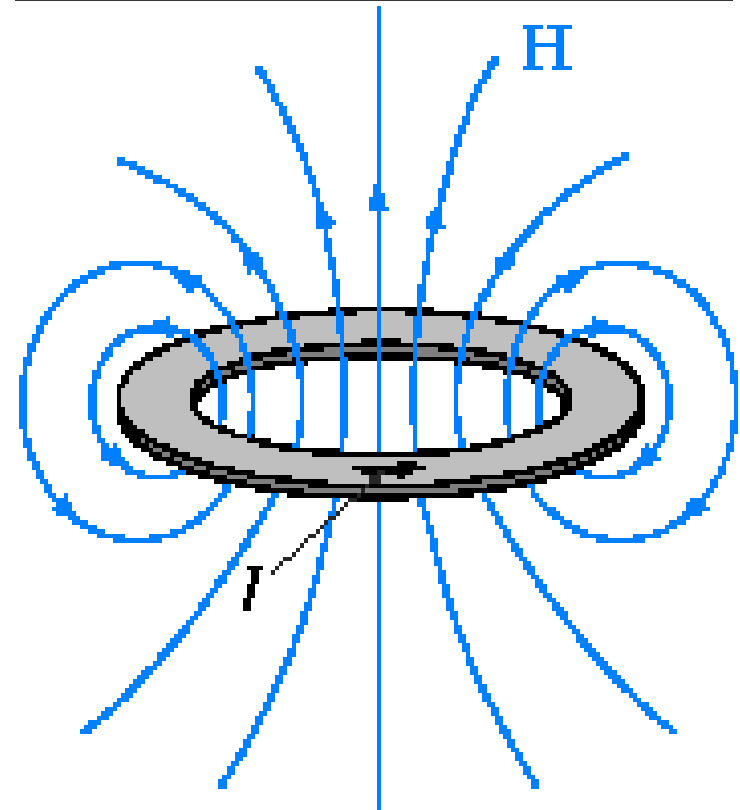
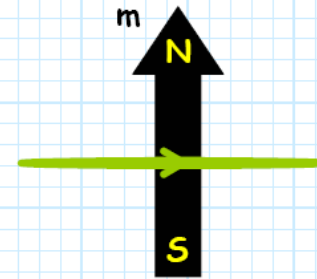




# Dipoles



Instead of plus (+) and minus (-), the **poles** of a magnetic dipole are defined as **north (N)** and **south (S)**:



# Biot-Savart

(note: just a name)

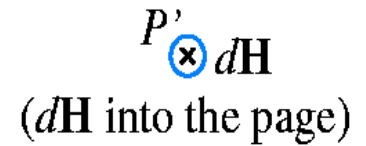
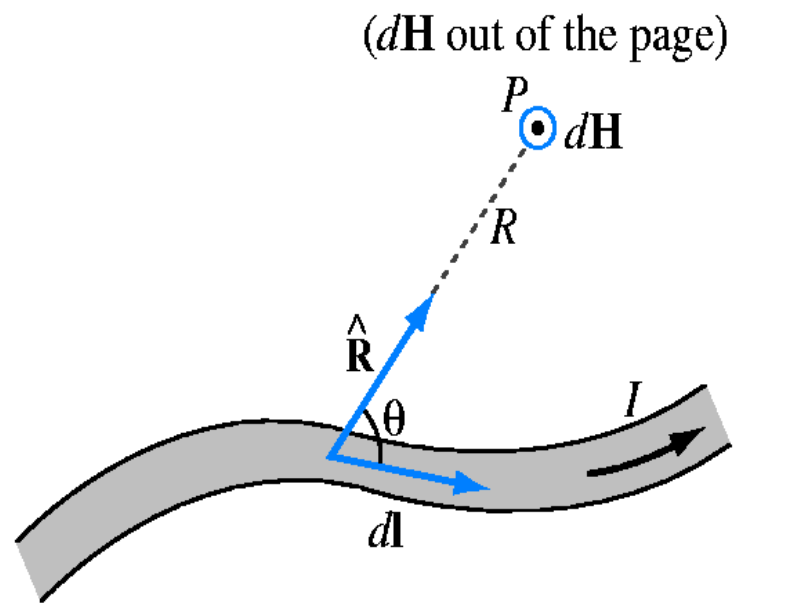
$$d\vec{H} = \frac{I}{4\pi} \cdot \frac{d\vec{\ell} \times \hat{R}}{R^2}$$

Add It up

$$\vec{H} = \frac{I}{4\pi} \int_{\ell} \frac{d\vec{\ell} \times \hat{R}}{R^2}$$

OR

$$\vec{H} = \frac{I}{4\pi} \int_S \frac{\vec{J}_s \times \hat{R}}{R^2} ds$$

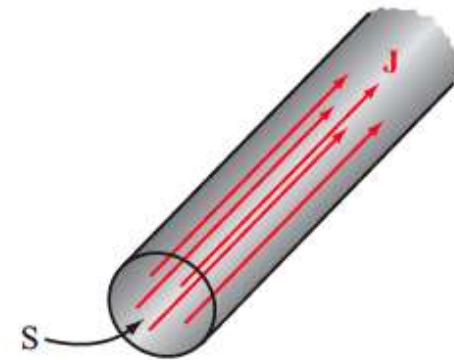




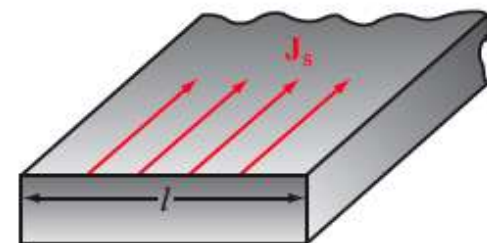
# Magnetic Field due to Current Densities

$$\mathbf{H} = \frac{1}{4\pi} \int_S \frac{\mathbf{J}_s \times \hat{\mathbf{R}}}{R^2} ds \quad (\text{surface current}),$$

$$\mathbf{H} = \frac{1}{4\pi} \int_V \frac{\mathbf{J} \times \hat{\mathbf{R}}}{R^2} dV \quad (\text{volume current}).$$



(a) Volume current density  $\mathbf{J}$  in A/m<sup>2</sup>



(b) Surface current density  $\mathbf{J}_s$  in A/m

**Figure 5-9:** (a) The total current crossing the cross section  $S$  of the cylinder is  $I = \int_S \mathbf{J} \cdot d\mathbf{s}$ . (b) The total current flowing across the surface of the conductor is  $I = \int_l J_s dl$ .

# Example 5-2: Magnetic Field of Linear Conductor

**Solution:** From Fig. 5-10, the differential length vector  $d\mathbf{l} = \hat{\mathbf{z}} dz$ . Hence,  $d\mathbf{l} \times \hat{\mathbf{R}} = dz (\hat{\mathbf{z}} \times \hat{\mathbf{R}}) = \hat{\boldsymbol{\phi}} \sin \theta dz$ , where  $\hat{\boldsymbol{\phi}}$  is the azimuth direction and  $\theta$  is the angle between  $d\mathbf{l}$  and  $\hat{\mathbf{R}}$ . Application of Eq. (5.22) gives

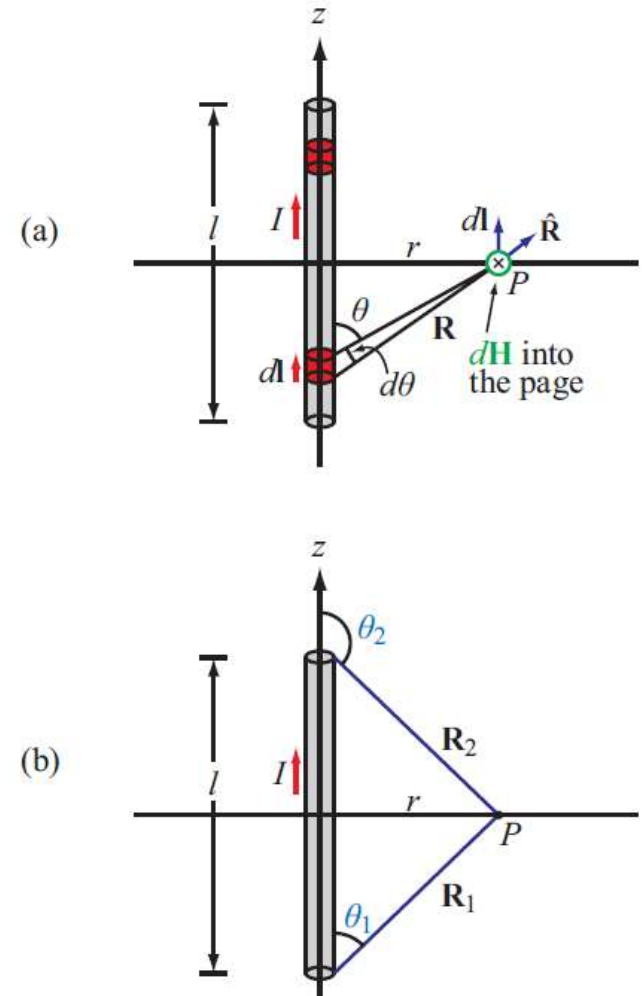
$$\mathbf{H} = \frac{I}{4\pi} \int_{z=-l/2}^{z=l/2} \frac{d\mathbf{l} \times \hat{\mathbf{R}}}{R^2} = \hat{\boldsymbol{\phi}} \frac{I}{4\pi} \int_{-l/2}^{l/2} \frac{\sin \theta}{R^2} dz. \quad (5.25)$$

Both  $R$  and  $\theta$  are dependent on the integration variable  $z$ , but the radial distance  $r$  is not. For convenience, we will convert the integration variable from  $z$  to  $\theta$  by using the transformations

$$R = r \csc \theta, \quad (5.26a)$$

$$z = -r \cot \theta, \quad (5.26b)$$

$$dz = r \csc^2 \theta d\theta. \quad (5.26c)$$



**Figure 5-10:** Linear conductor of length  $l$  carrying a current  $I$ . (a) The field  $d\mathbf{H}$  at point  $P$  due to incremental current element  $d\mathbf{l}$ . (b) Limiting angles  $\theta_1$  and  $\theta_2$ , each measured between vector  $I d\mathbf{l}$  and the vector connecting the end of the conductor associated with that angle to point  $P$  (Example 5-2).

Cont.

Upon inserting Eqs. (5.26a) and (5.26c) into Eq. (5.25), we have

$$\begin{aligned} \mathbf{H} &= \hat{\phi} \frac{I}{4\pi} \int_{\theta_1}^{\theta_2} \frac{\sin \theta \, r \csc^2 \theta \, d\theta}{r^2 \csc^2 \theta} \\ &= \hat{\phi} \frac{I}{4\pi r} \int_{\theta_1}^{\theta_2} \sin \theta \, d\theta \\ &= \hat{\phi} \frac{I}{4\pi r} (\cos \theta_1 - \cos \theta_2), \end{aligned} \quad (5.27)$$

where  $\theta_1$  and  $\theta_2$  are the limiting angles at  $z = -l/2$  and  $z = l/2$ , respectively. From the right triangle in Fig. 5-10(b), it follows that

$$\cos \theta_1 = \frac{l/2}{\sqrt{r^2 + (l/2)^2}}, \quad (5.28a)$$

$$\cos \theta_2 = -\cos \theta_1 = \frac{-l/2}{\sqrt{r^2 + (l/2)^2}}. \quad (5.28b)$$

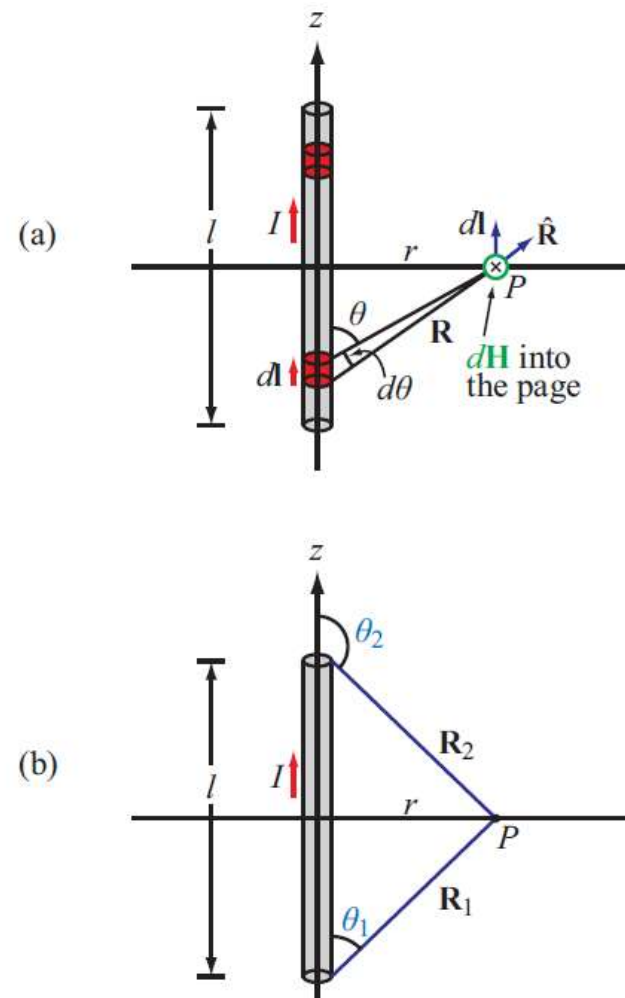
Hence,

$$\mathbf{B} = \mu_0 \mathbf{H} = \hat{\phi} \frac{\mu_0 I l}{2\pi r \sqrt{4r^2 + l^2}} \quad (\text{T}). \quad (5.29)$$

For an infinitely long wire with  $l \gg r$ , Eq. (5.29) reduces to

$$\mathbf{B} = \hat{\phi} \frac{\mu_0 I}{2\pi r} \quad (\text{infinitely long wire}). \quad (5.30)$$

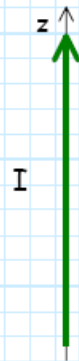
## Example 5-2: Magnetic Field of Linear Conductor



**Figure 5-10:** Linear conductor of length  $l$  carrying a current  $I$ . (a) The field  $d\mathbf{H}$  at point  $P$  due to incremental current element  $dI$ . (b) Limiting angles  $\theta_1$  and  $\theta_2$ , each measured between vector  $I \, dI$  and the vector connecting the end of the conductor associated with that angle to point  $P$  (Example 5-2).

# Example: The Uniform, Infinite Line of Current

Consider electric current  $I$  flowing along the  $z$ -axis from  $z = -\infty$  to  $z = \infty$ . What magnetic flux potential  $\mathbf{B}(\mathbf{r})$  is created by this current?

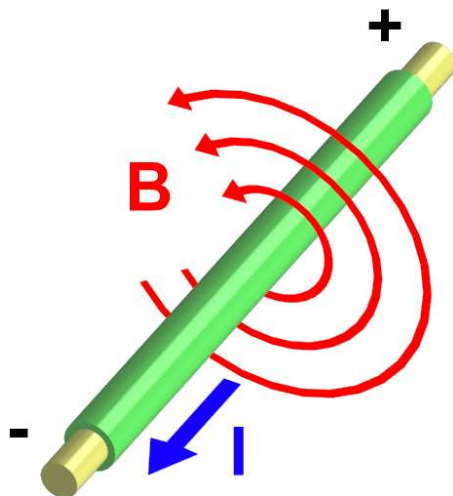


$$d\mathbf{l} = \hat{a}_z dz'$$

$$\begin{aligned}\mathbf{r} &= x \hat{a}_x + y \hat{a}_y + z \hat{a}_z \\ &= \rho \cos\phi \hat{a}_x + \rho \sin\phi \hat{a}_y + z \hat{a}_z\end{aligned}$$

$$\mathbf{r}' = z' \hat{a}_z \quad (x' = 0, y' = 0)$$

$$\begin{aligned}|\mathbf{r} - \mathbf{r}'| &= \sqrt{\rho^2 \cos^2\phi + \rho^2 \sin^2\phi + (z - z')^2} \\ &= \sqrt{\rho^2 + (z - z')^2}\end{aligned}$$



We can determine the magnetic flux density by applying the Biot-Savart Law:

$$\begin{aligned}\mathbf{B}(\mathbf{r}) &= \frac{\mu_0 I}{4\pi} \oint \frac{d\mathbf{l}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} \\ &= \frac{\mu_0 I}{4\pi} \int_{-\infty}^{\infty} \frac{\hat{a}_z \times [\rho \cos\phi \hat{a}_x + \rho \sin\phi \hat{a}_y + (z - z') \hat{a}_z]}{[\rho^2 + (z - z')^2]^{3/2}} dz' \\ &= \frac{\mu_0 I}{4\pi} \int_{-\infty}^{\infty} \frac{\rho \cos\phi \hat{a}_y - \rho \sin\phi \hat{a}_x}{[\rho^2 + (z - z')^2]^{3/2}} dz' \\ &= \frac{\mu_0 I}{4\pi} (\rho \cos\phi \hat{a}_y - \rho \sin\phi \hat{a}_x) \int_{-\infty}^{\infty} \frac{du}{[\rho^2 + u^2]^{3/2}} \\ &= \frac{\mu_0 I}{4\pi} (\rho \hat{a}_\phi) \left[ \frac{u}{\rho^2 \sqrt{\rho^2 + u^2}} \right]_{-\infty}^{\infty} \\ &= \frac{\mu_0 I}{4\pi} (\rho \hat{a}_\phi) \frac{2}{\rho^2} \\ &= \frac{\mu_0 I}{2\pi \rho} \hat{a}_\phi\end{aligned}$$

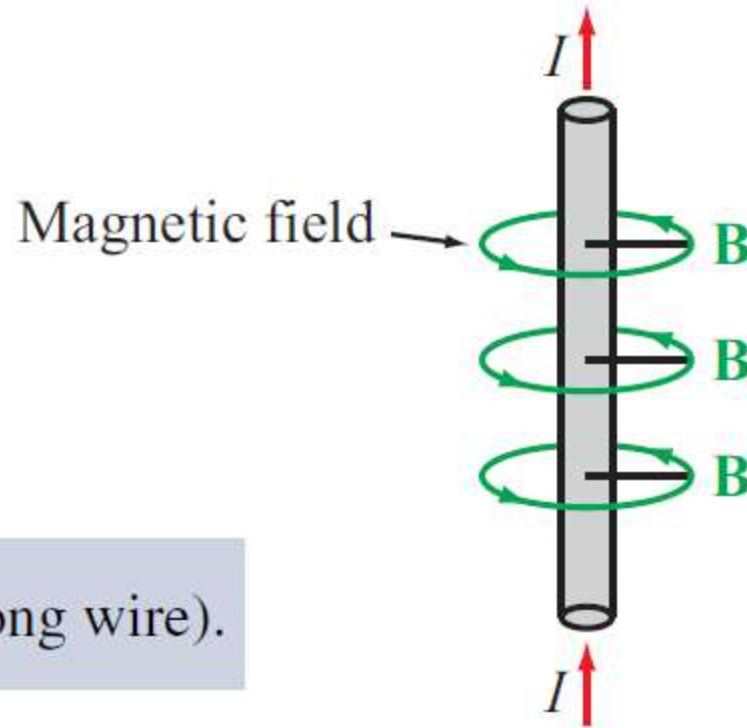
Therefore, the magnetic flux density **created** by a "wire" with current  $I$  flowing along the  $z$ -axis is:

$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0 I}{2\pi \rho} \hat{a}_\phi$$



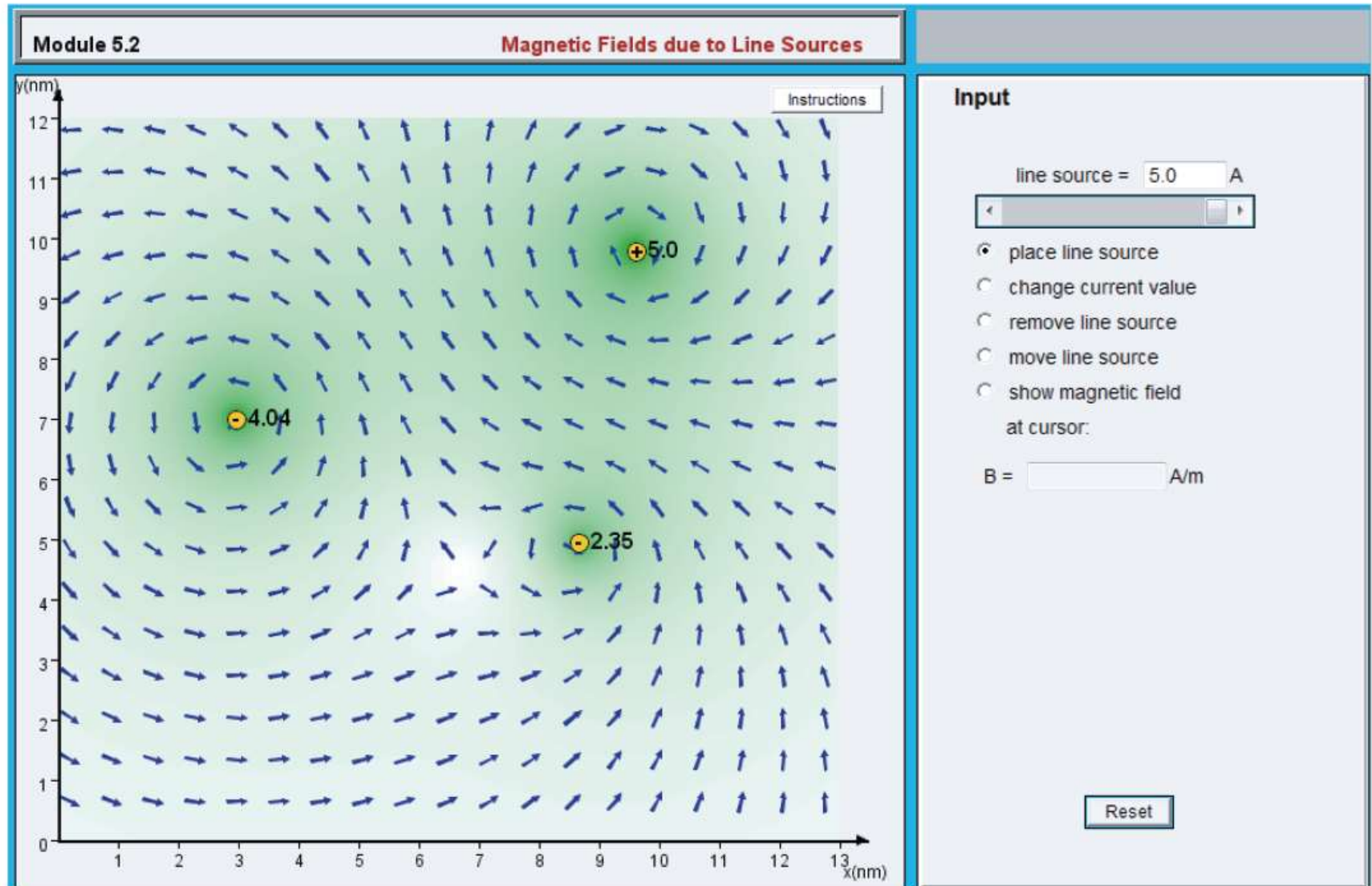
# Magnetic Field of Long Conductor

$$\mathbf{B} = \hat{\phi} \frac{\mu_0 I}{2\pi r} \quad (\text{infinitely long wire}).$$



## CD Module 5.2 Magnetic Fields due to Line Sources

You can place z-directed linear currents anywhere in the display plane ( $x$ - $y$  plane), select their magnitudes and directions, and then observe the spatial pattern of the induced magnetic flux  $\mathbf{B}(x, y)$ .



# Example 5-3: Magnetic Field of a Loop

Magnitude of field due to  $d\mathbf{l}$  is

$$dH = \frac{I}{4\pi R^2} |d\mathbf{l} \times \hat{\mathbf{R}}| = \frac{I dl}{4\pi (a^2 + z^2)}$$

$d\mathbf{H}$  is in the  $r$ - $z$  plane, and therefore it has components  $dH_r$  and  $dH_z$

**z-components** of the magnetic fields due to  $d\mathbf{l}$  and  $d\mathbf{l}'$  **add** because they are in the same direction, but their **r-components** **cancel**

Hence for element  $d\mathbf{l}$ :

$$d\mathbf{H} = \hat{\mathbf{z}} dH_z = \hat{\mathbf{z}} dH \cos \theta = \hat{\mathbf{z}} \frac{I \cos \theta}{4\pi (a^2 + z^2)} dl$$

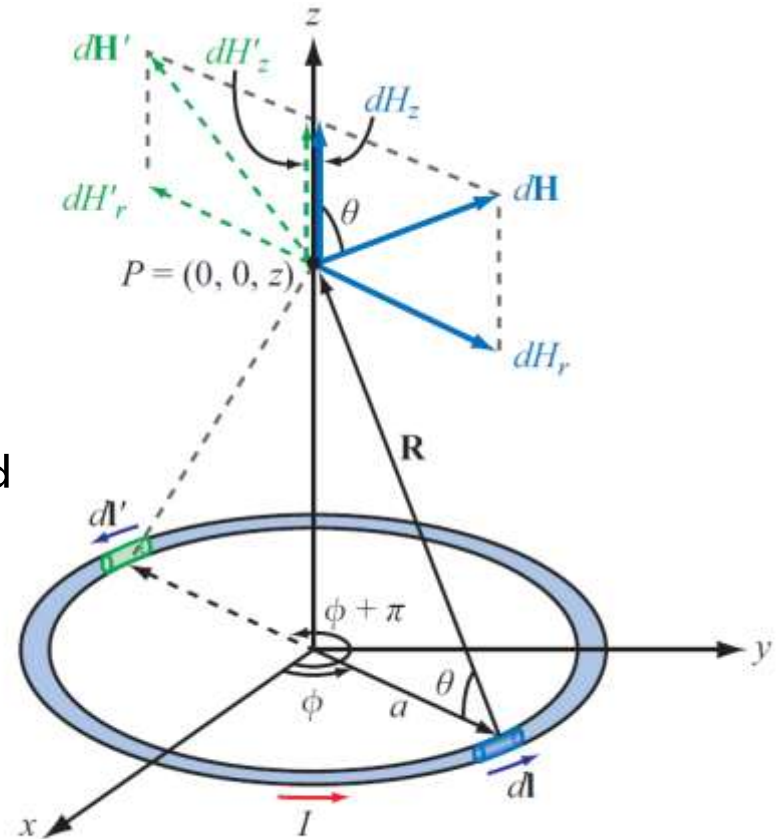


Figure 5-12: Circular loop carrying a current  $I$  (Example 5-3).

# Example 5-3: Magnetic Field of a Loop (cont.)

For the entire loop:

$$\mathbf{H} = \hat{\mathbf{z}} \frac{I \cos \theta}{4\pi(a^2 + z^2)} \oint dl = \hat{\mathbf{z}} \frac{I \cos \theta}{4\pi(a^2 + z^2)} (2\pi a). \quad (5.33)$$

Upon using the relation  $\cos \theta = a/(a^2 + z^2)^{1/2}$ , we obtain

$$\mathbf{H} = \hat{\mathbf{z}} \frac{Ia^2}{2(a^2 + z^2)^{3/2}} \quad (\text{A/m}). \quad (5.34)$$

At the center of the loop ( $z = 0$ ), Eq. (5.34) reduces to

$$\mathbf{H} = \hat{\mathbf{z}} \frac{I}{2a} \quad (\text{at } z = 0), \quad (5.35)$$

and at points very far away from the loop such that  $z^2 \gg a^2$ , Eq. (5.34) simplifies to

$$\mathbf{H} = \hat{\mathbf{z}} \frac{Ia^2}{2|z|^3} \quad (\text{at } |z| \gg a). \quad (5.36)$$

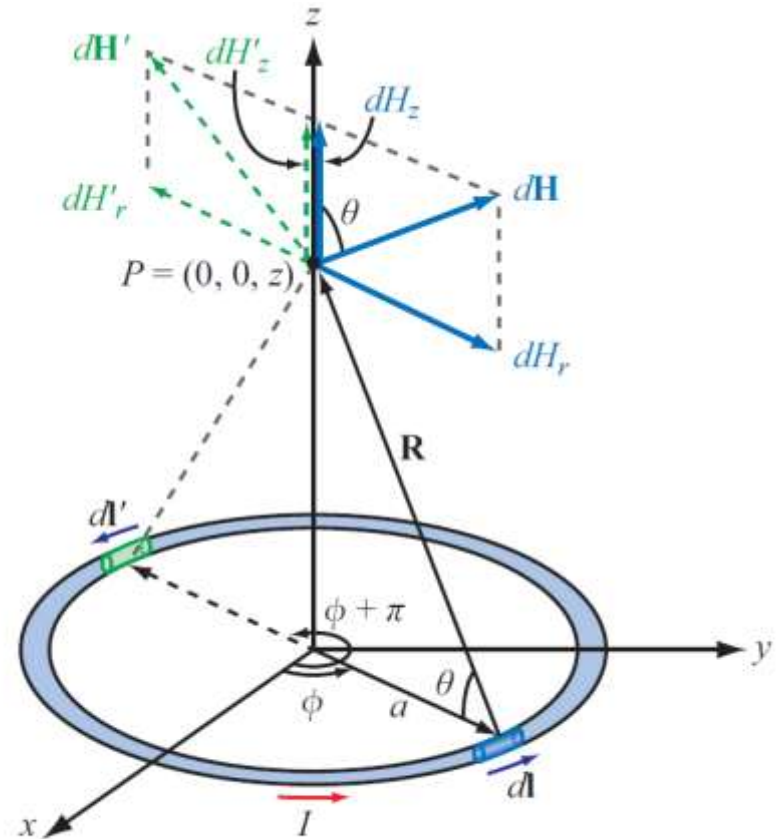


Figure 5-12: Circular loop carrying a current  $I$  (Example 5-3).

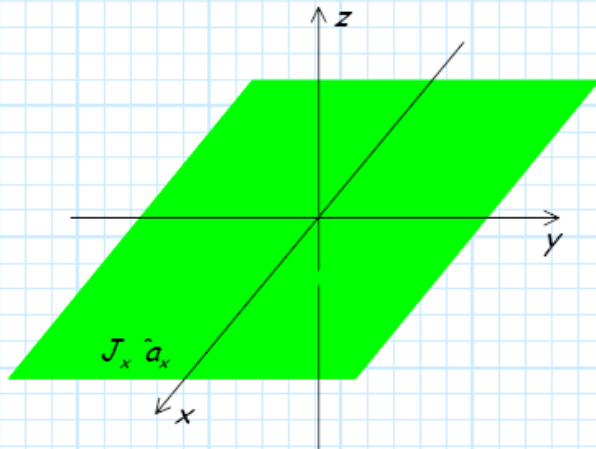


# B-Field from an Infinite Sheet of Current

Consider now an **infinite sheet** of current, lying on the  $z = 0$  plane. Say the surface current density on this sheet has a value:

$$\mathbf{J}_s(\bar{r}) = J_x \hat{a}_x$$

meaning that the current density at every point on the surface has the same magnitude, and flows in the  $\hat{a}_x$  direction.

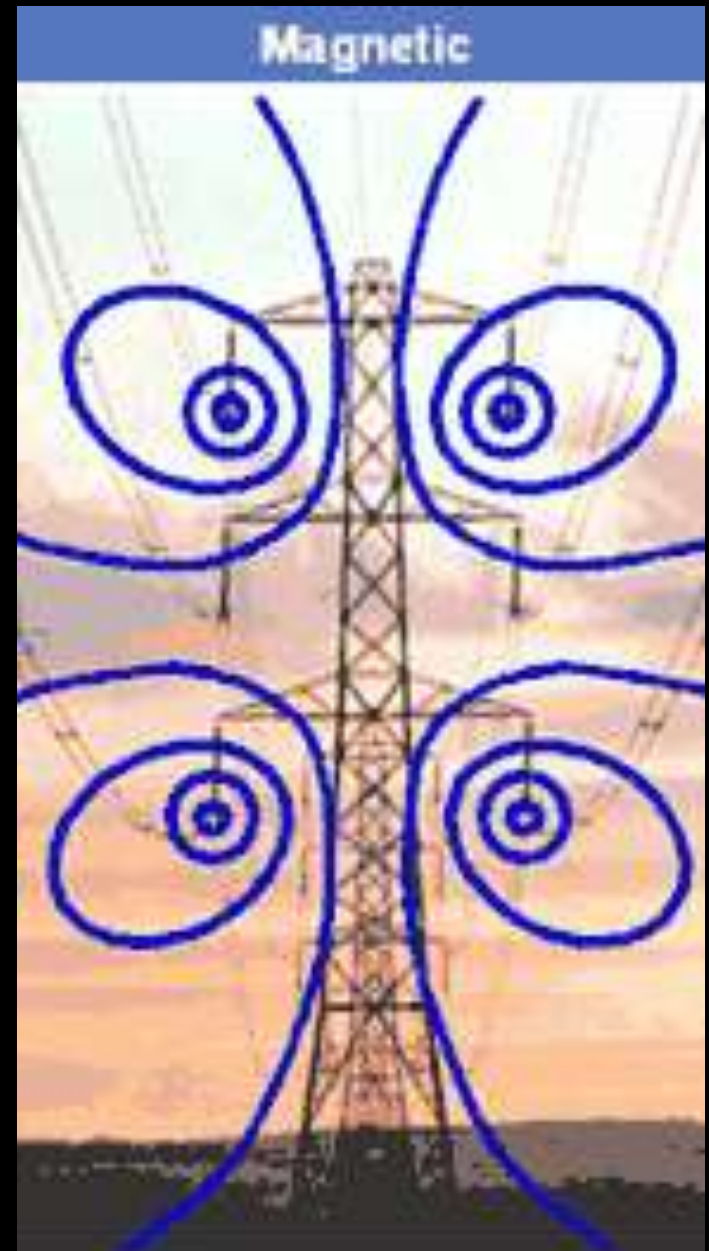
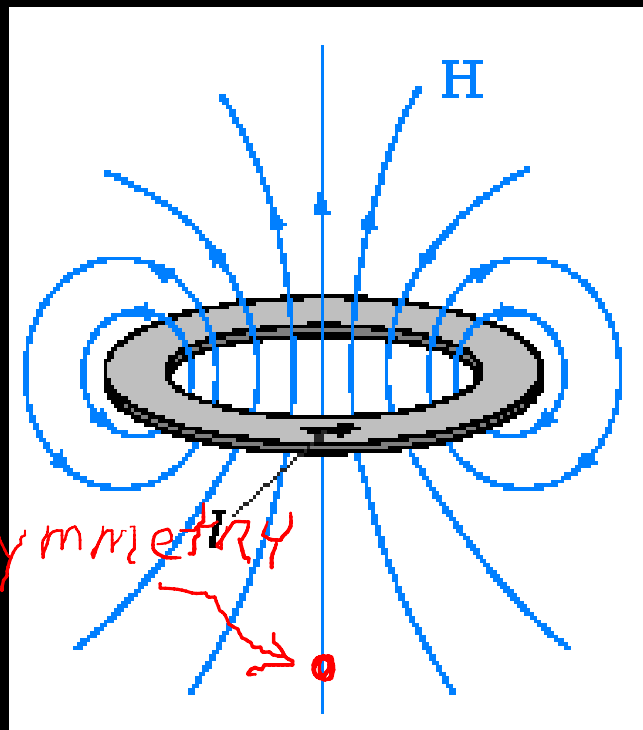
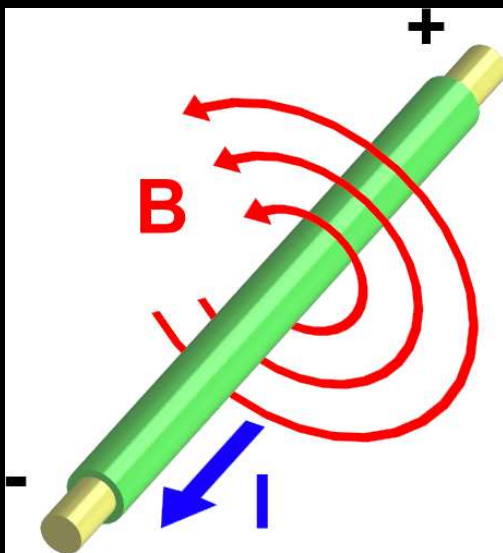


Using the Biot-Savart Law, we find that the magnetic flux density produced by this **infinite** current sheet is:

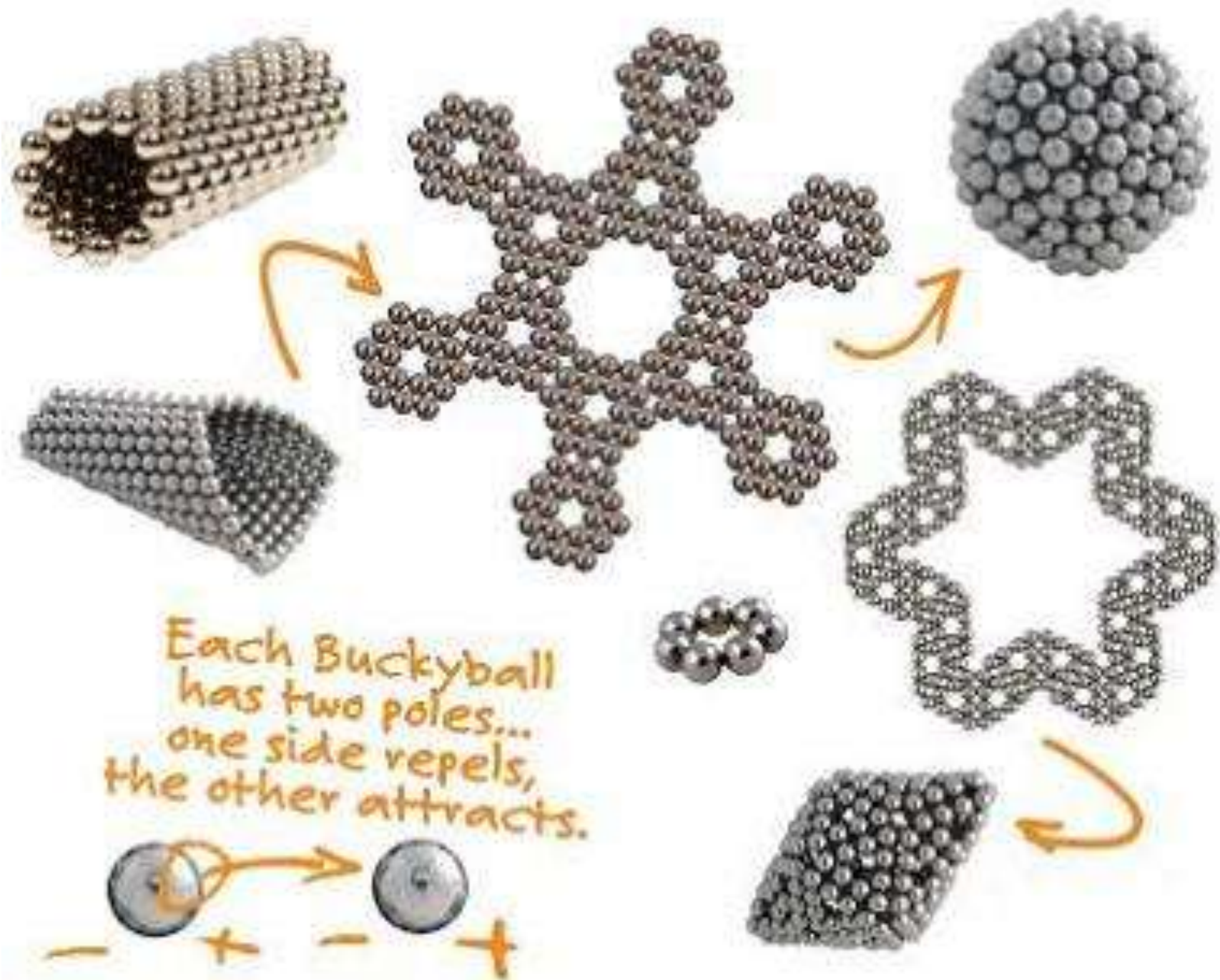
$$\mathbf{B}(\bar{r}) = \begin{cases} -\frac{\mu_0 J_x}{2} \hat{a}_y & z > 0 \\ \frac{\mu_0 J_x}{2} \hat{a}_y & z < 0 \end{cases}$$

Think about what this expression is telling us.

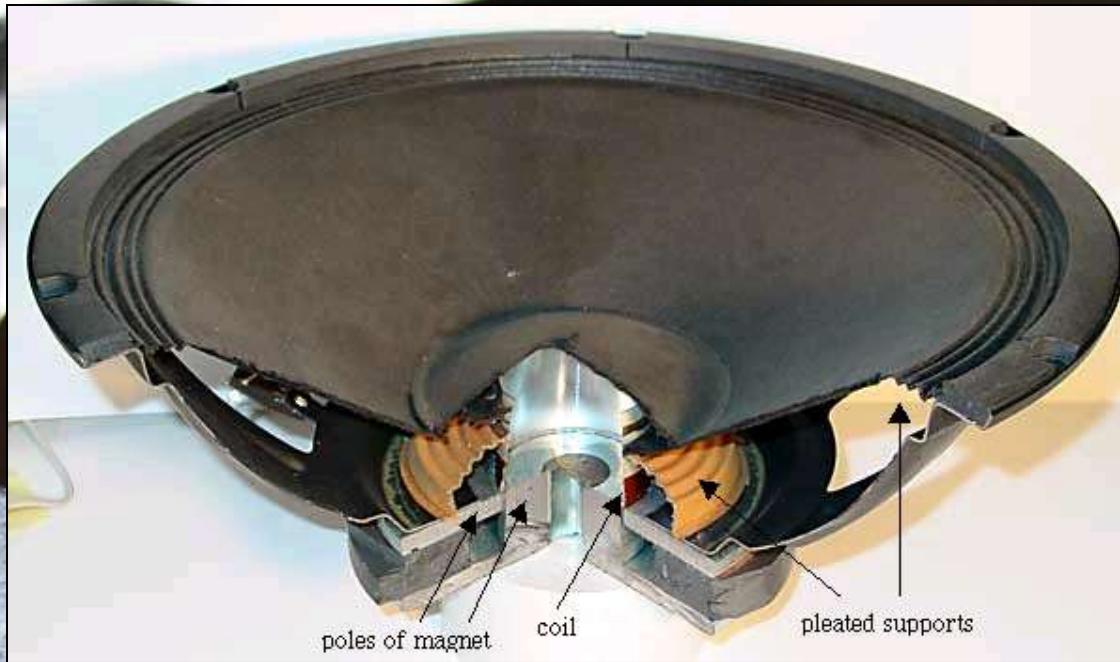
- ★ The magnitude of this magnetic flux density is a **constant**. In other words,  $\mathbf{B}(\bar{r})$  is **just** as large a million miles from the infinite current sheet as it is 1 millimeter from the current sheet!
- ★ The **direction** of the magnetic flux density in the  $-\hat{a}_y$  direction **above** the current sheet, but points in the **opposite** direction (i.e.,  $\hat{a}_y$ ) **below** it.
- ★ The direction of the magnetic flux density is **orthogonal** to the direction of current flow  $\hat{a}_x$ .







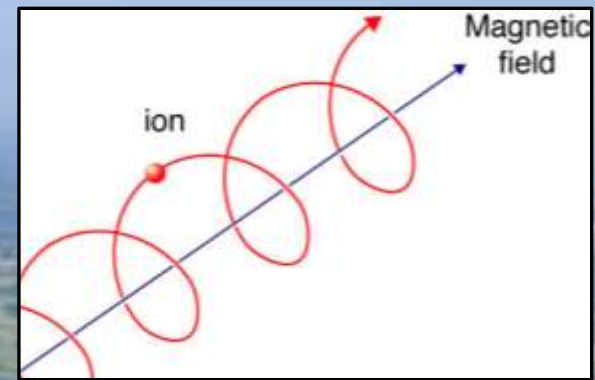
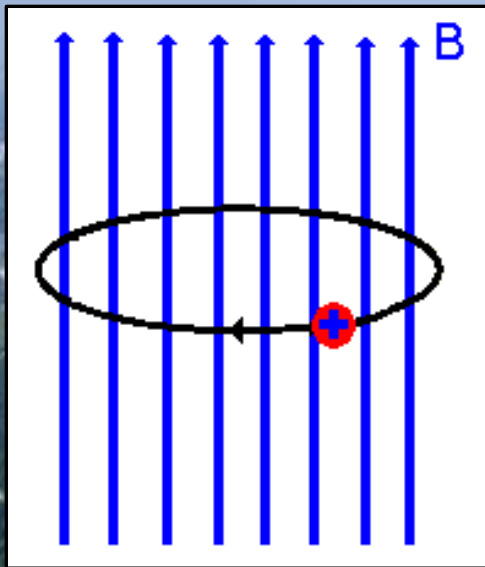




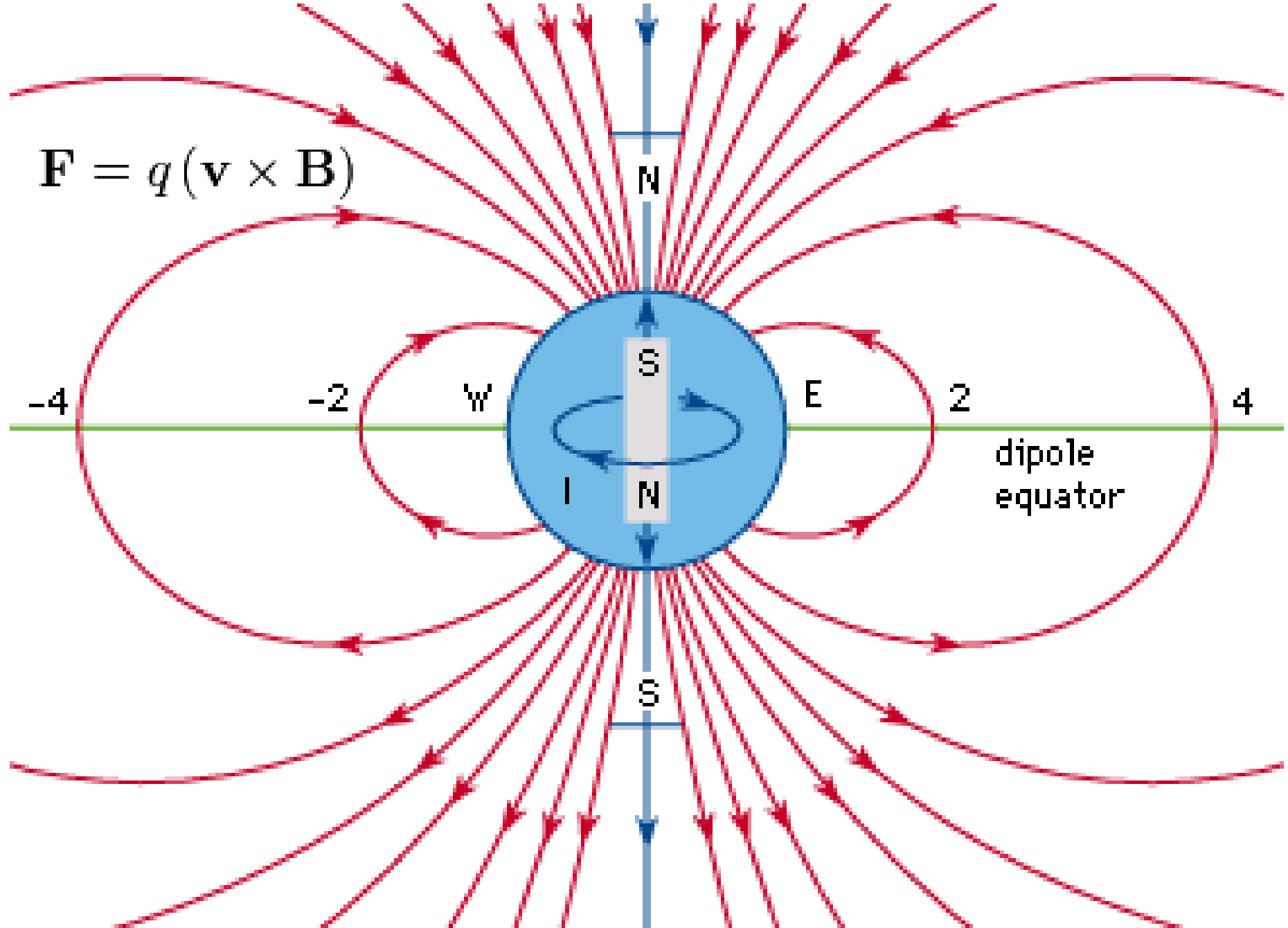
Attribute	Electrostatics	Magnetostatics
Sources	Stationary charges	Steady currents
Fields	$\mathbf{E}$ and $\mathbf{D}$	$\mathbf{H}$ and $\mathbf{B}$
Constitutive parameter(s)	$\epsilon$ and $\sigma$	$\mu$
Governing equations <ul style="list-style-type: none"> <li>Differential form</li> <li>Integral form</li> </ul>	$\nabla \cdot \mathbf{D} = \rho_v$ $\nabla \times \mathbf{E} = 0$ $\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$ $\oint_C \mathbf{E} \cdot d\mathbf{l} = 0$	$\nabla \cdot \mathbf{B} = 0$ $\nabla \times \mathbf{H} = \mathbf{J}$ $\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$ $\oint_C \mathbf{H} \cdot d\mathbf{l} = I$
Potential	Scalar $V$ , with $\mathbf{E} = -\nabla V$	Vector $\mathbf{A}$ , with $\mathbf{B} = \nabla \times \mathbf{A}$
Energy density	$w_e = \frac{1}{2} \epsilon E^2$	$w_m = \frac{1}{2} \mu H^2$
Force on charge $q$	$\mathbf{F}_e = q\mathbf{E}$	$\mathbf{F}_m = q\mathbf{u} \times \mathbf{B}$
Circuit element(s)	$C$ and $R$	$L$

$\mathbf{B} = \mu \mathbf{H}$





$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$



Magnetic field lines point from **North** to **South**



units of  $\vec{B}$  are  $\frac{N}{A \cdot m} = T$   
teslas

$$\mu_0 = 4\pi \times 10^{-7} \text{ N/A}^2$$

$$\vec{H} = \frac{I}{4\pi} \oint_C \frac{d\vec{\ell} \times \hat{R}}{R^2}$$

## Gauss

$$\nabla \cdot \mathbf{B} = 0$$

closed Loop  
field Lines

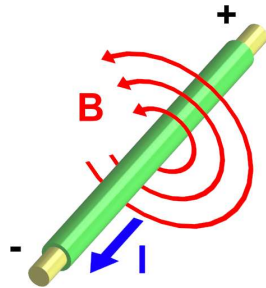
$$\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$$

## Ampere

$$\nabla \times \mathbf{H} = \mathbf{J}$$

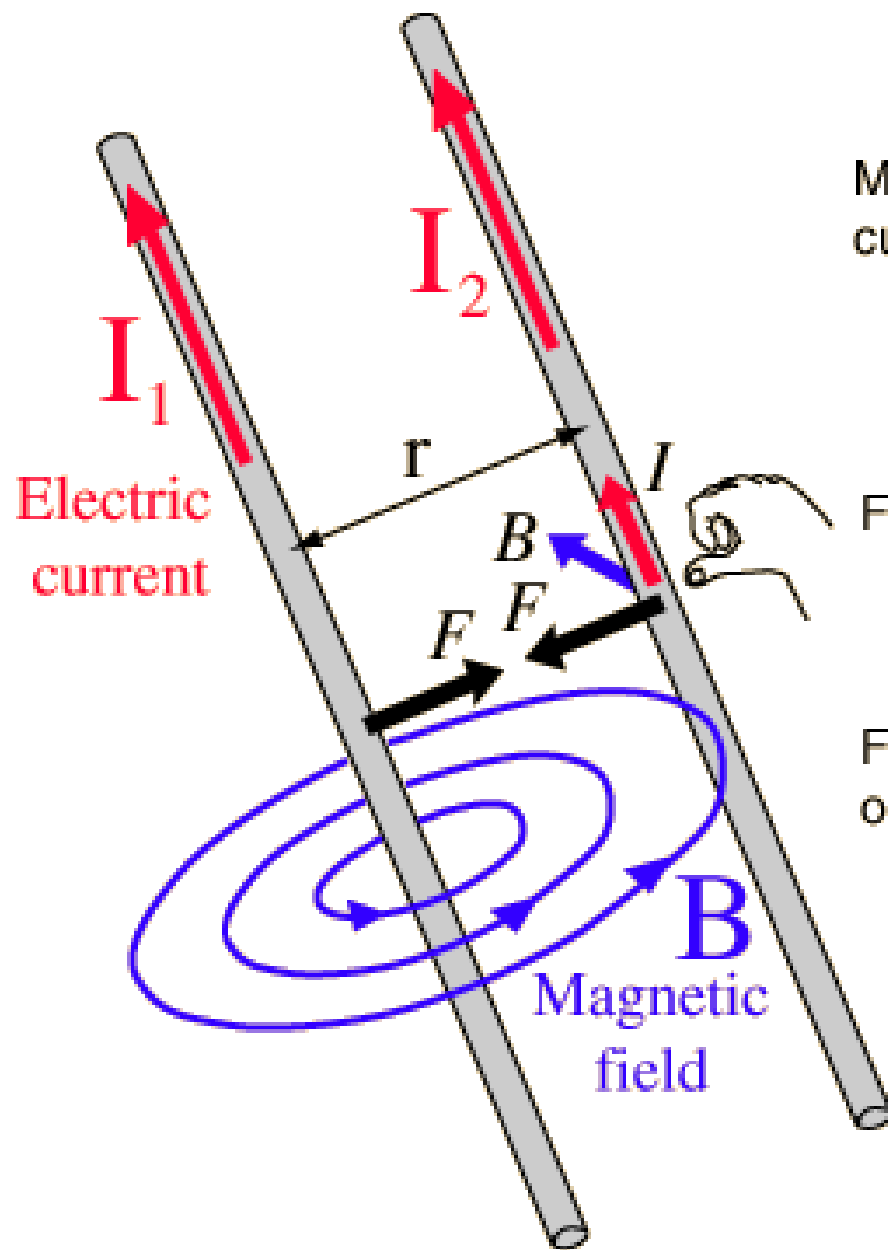
$$\oint_C \mathbf{H} \cdot d\mathbf{l} = I$$

Example Infinite wire



$$\Rightarrow \oint_C \frac{\vec{B}}{\mu} \cdot d\vec{l} = \frac{2\pi r B_\phi}{\mu} = I$$

$$\Rightarrow \vec{B} = \frac{\mu I}{2\pi r} \hat{\phi} \quad \text{T as before}$$



Magnetic field at wire 2 from current in wire 1:

$$B = \frac{\mu_0 I_1}{2\pi r}$$

Force on a length  $\Delta L$  of wire 2:

$$F = I_2 \Delta L B$$

Force per unit length in terms of the currents:

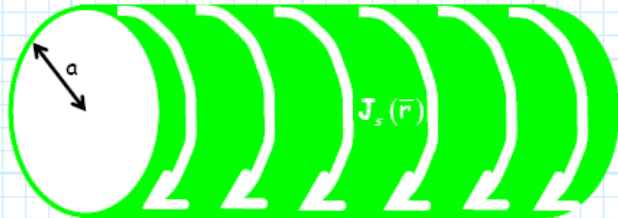
$$\frac{F}{\Delta L} = \frac{\mu_0 I_1 I_2}{2\pi r}$$

Remember the force between plates in a capacitor?  
Hmmm.... ☺

# Solenoids

An important structure in electrical and computer engineering is the **solenoid**.

A solenoid is a **tube of current**. However, it is different from the hollow cylinder example, in that the current flows **around** the tube, rather than down the tube:

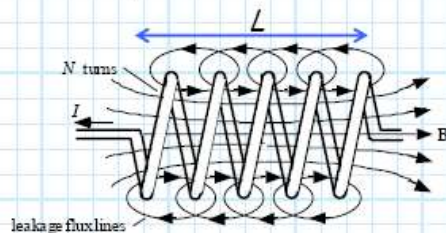


Aligning the center of the tube with the  $z$ -axis, we can express the **current density** as:

$$\mathbf{J}_s(\vec{r}) = \begin{cases} 0 & \rho < a \\ J_s \hat{a}_\phi & \rho = a \\ 0 & \rho > a \end{cases} \quad \left[ \frac{\text{Amps}}{\text{m}} \right]$$

where  $a$  is the **radius** of the solenoid, and  $J_s$  is the **surface current** density

**A:** We can easily make a solenoid by forming a **wire spiral** around a cylinder.



We can use **Ampere's Law** to find the magnetic flux density resulting from this structure. The result is:

$$\mathbf{B}(\vec{r}) = \begin{cases} \mu_0 J_s \hat{a}_z & \rho < a \\ 0 & \rho > a \end{cases}$$

Note the direction of the magnetic flux density is in the direction  $\hat{a}_z$ --it points **down** the center of the solenoid.

Note also that the magnitude  $|\mathbf{B}(\vec{r})|$  is **independent** of solenoid radius  $a$ !

The surface current density  $J_s$  of this solenoid is **approximately** equal to:

$$J_s = \frac{N I}{L} = N_\ell I$$

where  $N_\ell = N/L$  is the number of turns/unit length. Inserting this result into our expression for magnetic flux density, we find the magnetic flux density **inside** a solenoid:

$$\begin{aligned} \mathbf{B}(\vec{r}) &= \mu_0 \frac{N I}{L} \hat{a}_z \\ &= \mu_0 N_\ell I \hat{a}_z \end{aligned}$$



### Example:

Find the magnetic field of a very long solenoid.

#### **Solenoid:**

$N$  turns of wire wound around a straight core with cylindrical or rectangular cross section.

When  $l \gg a$ , we can neglect the fringing effects at both ends of the solenoid and view it as a toroid with an infinitely large radius. Then, the magnetic field is confined within the solenoid's core and is given by

$$H_z = \frac{NI}{l} = nI, \quad n = \frac{N}{l}$$

– turns per unit length

$$\vec{H} = \hat{z} \frac{NI}{l} = \hat{z} nI$$

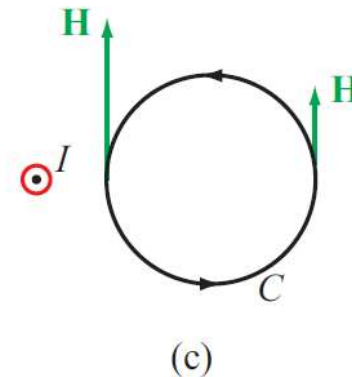
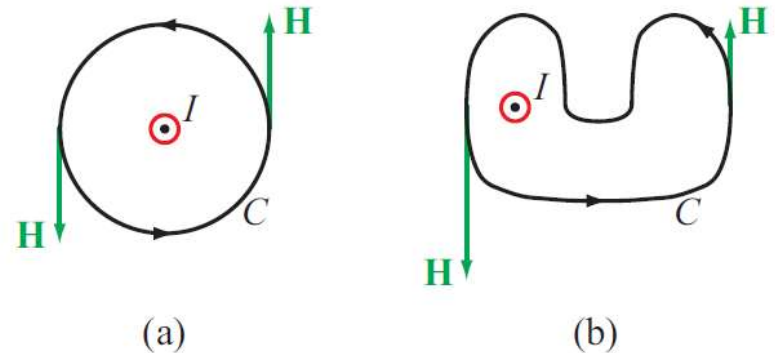
**The field of a long solenoid is uniform in first approximation.**





# Ampère's Law

$$\nabla \times \mathbf{H} = \mathbf{J} \quad \longleftrightarrow \quad \oint_C \mathbf{H} \cdot d\boldsymbol{\ell} = I$$



*The sign convention for the direction of the contour path  $C$  in Ampère's law is taken so that  $I$  and  $\mathbf{H}$  satisfy the right-hand rule defined earlier in connection with the Biot–Savart law. That is, if the direction of  $I$  is aligned with the direction of the thumb of the right hand, then the direction of the contour  $C$  should be chosen along that of the other four fingers.*

**Figure 5-16:** Ampère's law states that the line integral of  $\mathbf{H}$  around a closed contour  $C$  is equal to the current traversing the surface bounded by the contour. This is true for contours (a) and (b), but the line integral of  $\mathbf{H}$  is zero for the contour in (c) because the current  $I$  (denoted by the symbol  $\odot$ ) is not enclosed by the contour  $C$ .

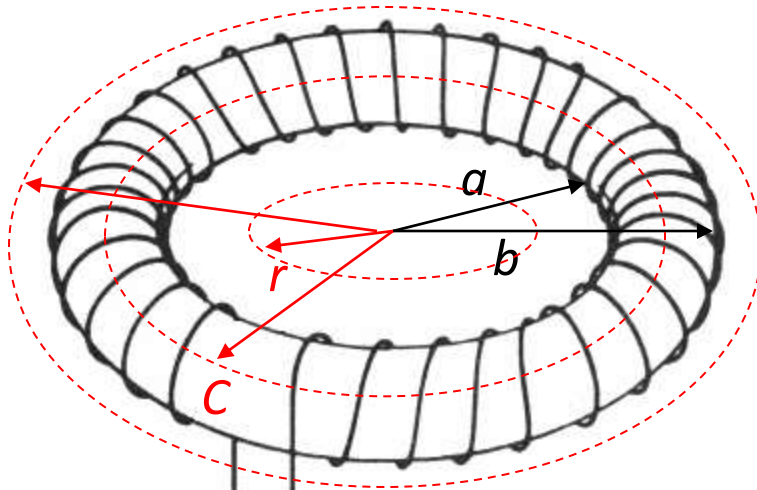
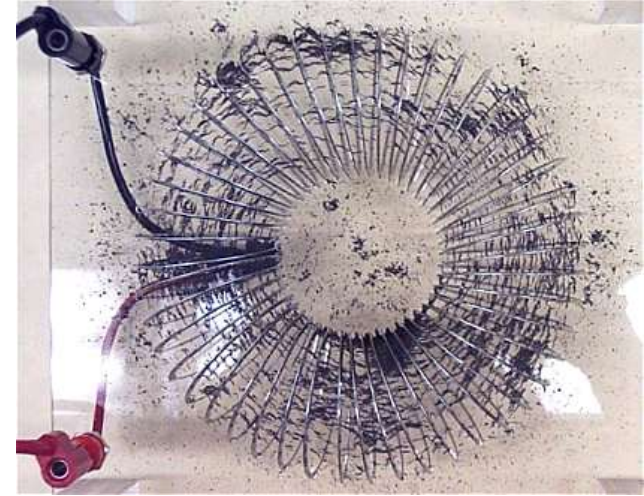


### Example:

Find the magnetic field of a toroidal coil.

**Toroid:**  $N$  turns of wire wound around a ring-like core.

$$\oint_C \vec{H} \cdot d\vec{l} = I$$



**Region 1:**  $r < a$

$$I = 0 \Rightarrow H = 0$$

**Region 2:**  $a < r < b$

$$\left. \begin{aligned} I_{total} &= NI \\ \oint_C \vec{H} \cdot d\vec{l} &= H_\phi 2\pi r \end{aligned} \right\} H_\phi = \frac{NI}{2\pi r}$$

$$\vec{H} = \hat{\phi} \frac{NI}{2\pi r}$$

**Region 3:**  $r > b$

$$I_{total} = NI - NI = 0 \Rightarrow H = 0$$





# Internal Magnetic Field of Long Conductor

For  $r < a$

$$\oint \mathbf{H}_1 \cdot d\mathbf{l}_1 = I_1,$$

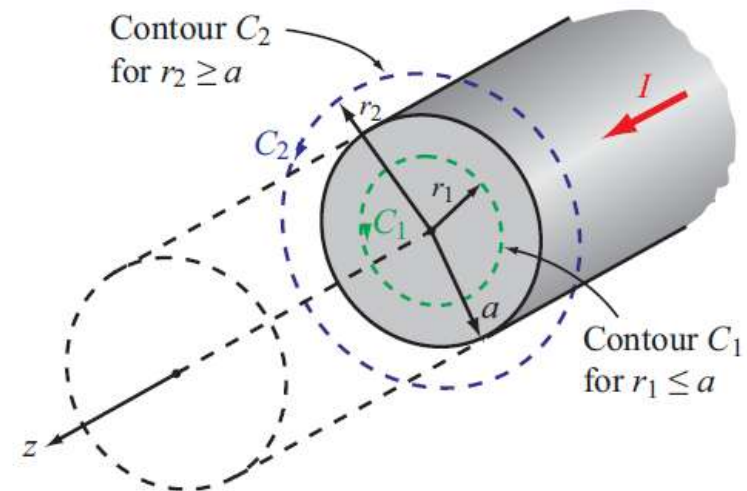
$$\oint_{C_1} \mathbf{H}_1 \cdot d\mathbf{l}_1 = \int_0^{2\pi} H_1 (\hat{\phi} \cdot \hat{\phi}) r_1 d\phi = 2\pi r_1 H_1.$$

The current  $I_1$  flowing through the area enclosed by  $C_1$  is equal to the total current  $I$  multiplied by the ratio of the area enclosed by  $C_1$  to the total cross-sectional area of the wire:

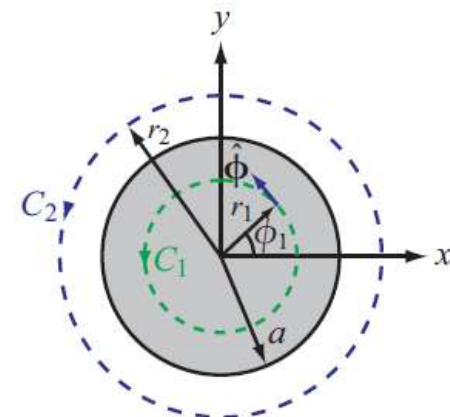
$$I_1 = \left( \frac{\pi r_1^2}{\pi a^2} \right) I = \left( \frac{r_1}{a} \right)^2 I.$$

Equating both sides of Eq. (5.48) and then solving for  $\mathbf{H}_1$  yields

$$\mathbf{H}_1 = \hat{\phi} H_1 = \hat{\phi} \frac{r_1}{2\pi a^2} I \quad (\text{for } r_1 \leq a). \quad (5.49a)$$



(a) Cylindrical wire

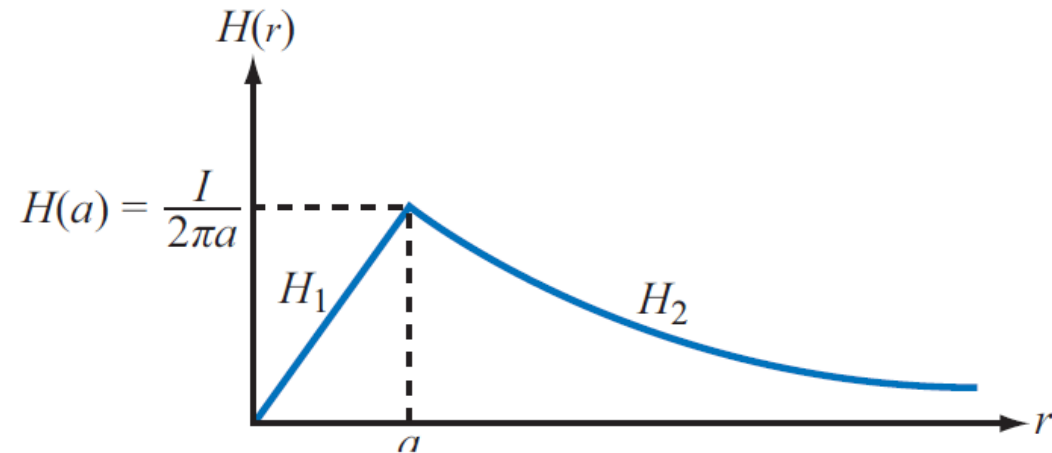


(b) Wire cross section

Cont.

# External Magnetic Field of Long Conductor

For  $r > a$

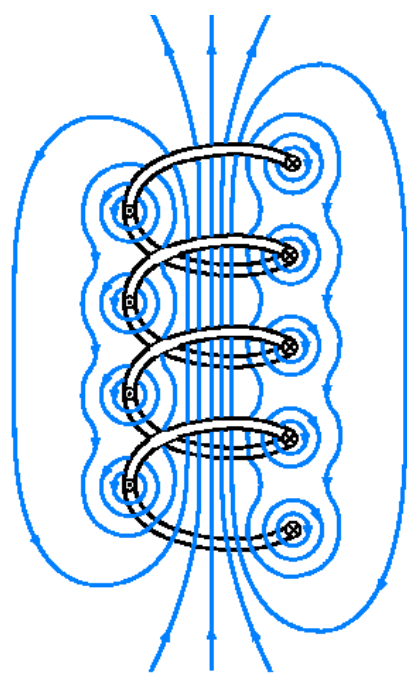


(b) For  $r = r_2 \geq a$ , we choose path  $C_2$ , which encloses all the current  $I$ . Hence,  $\mathbf{H}_2 = \hat{\phi} H_2$ ,  $d\mathbf{l}_2 = \hat{\phi} r_2 d\phi$ , and

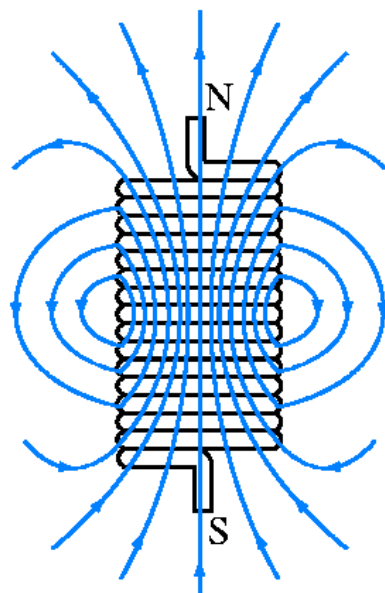
$$\oint_{C_2} \mathbf{H}_2 \cdot d\mathbf{l}_2 = 2\pi r_2 H_2 = I,$$

which yields

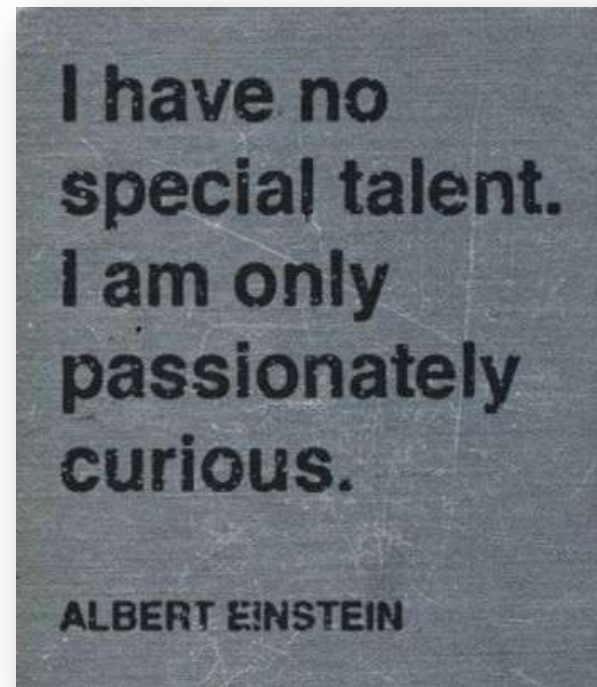
$$\mathbf{H}_2 = \hat{\phi} H_2 = \hat{\phi} \frac{I}{2\pi r_2} \quad (\text{for } r_2 \geq a). \quad (5.49b)$$



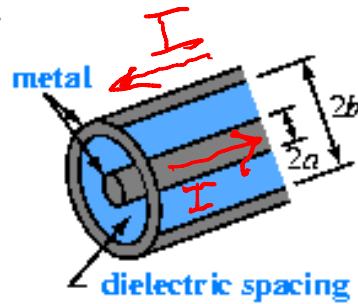
(a) Loosely wound solenoid



(b) Tightly wound solenoid



## Another Example



- What is  $\vec{B}$  outside of cable?
- What is  $\vec{B}$  between conductors?

## Vector Magnetic Potential

$$\mathbf{B} = \nabla \times \mathbf{A}$$

allows  $\nabla \cdot \vec{B} = 0$

units of  $\text{Wb/m}$   
(Webers)

$$\vec{A} = \frac{\mu}{4\pi} \int_V \frac{\vec{J}}{R} dv$$

Poisson

$$\nabla^2 \vec{A} = -\mu \vec{J}$$



# Magnetic Vector Potential **A**

## Electrostatics

$$\mathbf{E} = -\nabla V$$

$$\nabla^2 V = -\frac{\rho_v}{\epsilon}$$

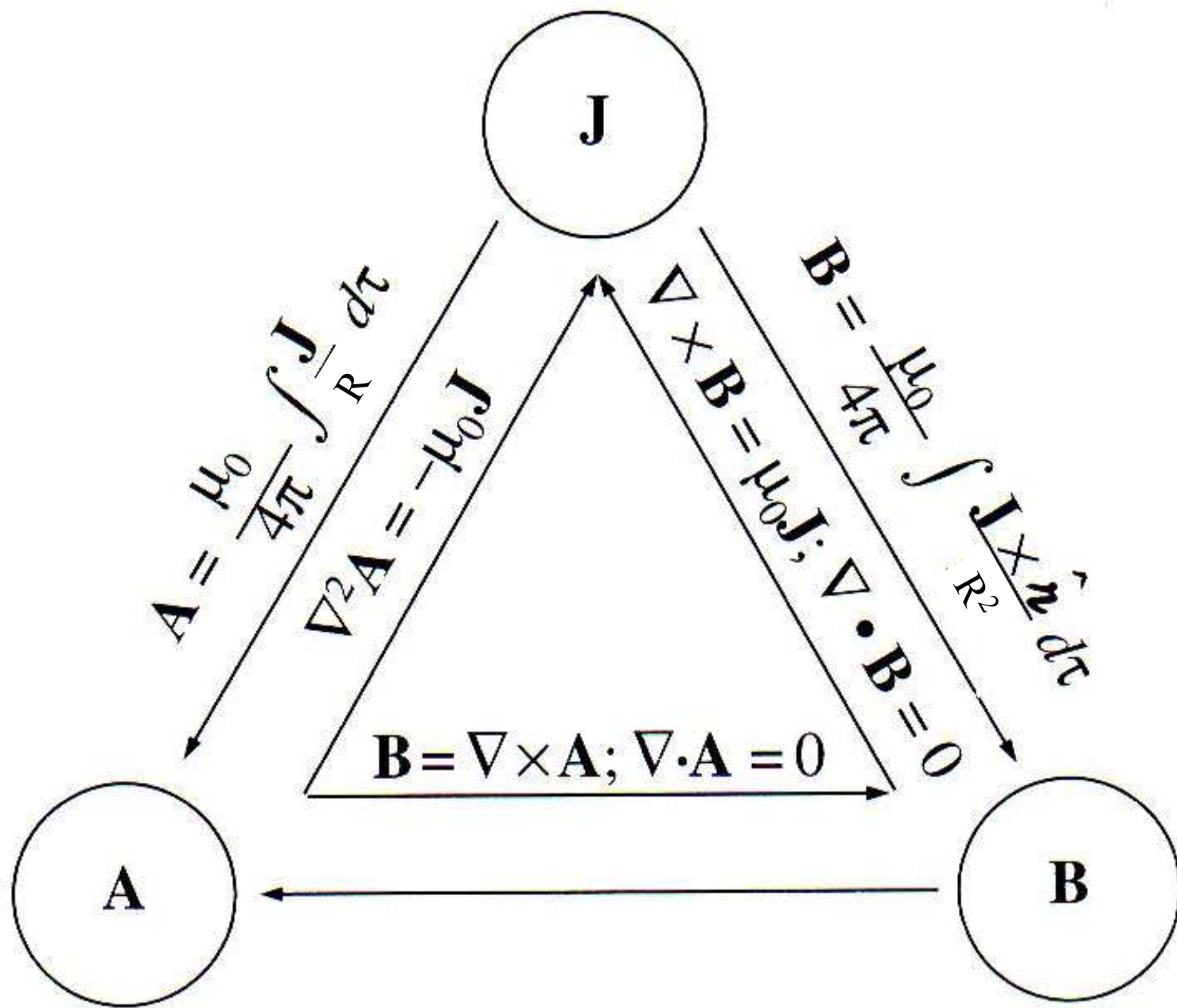
$$V = \frac{1}{4\pi\epsilon} \int_{V'} \frac{\rho_v}{R'} dV'$$

## Magnetostatics

$$\mathbf{B} = \nabla \times \mathbf{A} \quad (\text{Wb/m}^2),$$

$$\nabla^2 \mathbf{A} = -\mu \mathbf{J}.$$

$$\mathbf{A} = \frac{\mu}{4\pi} \int_{V'} \frac{\mathbf{J}}{R'} dV' \quad (\text{Wb/m}).$$



Note: in our text, some people call this field

$\vec{B}$  = magnetic flux density ( $\frac{N}{A \cdot m} = T$ )

$\vec{H}$  = magnetic field intensity ( $\frac{A}{m}$ )

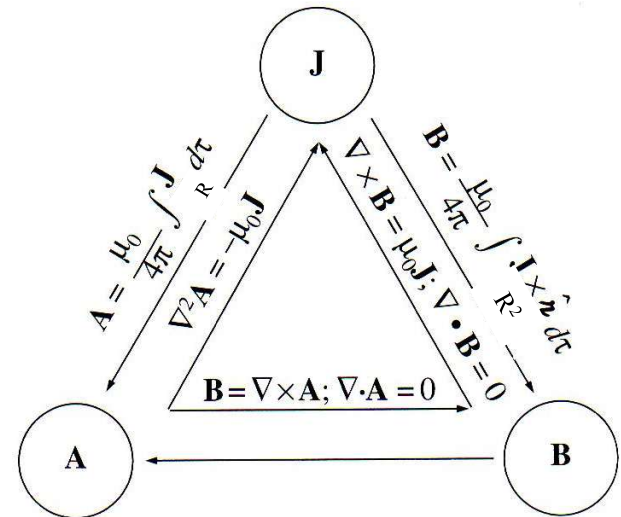
$$\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$$

1 Gauss =  $1 \times 10^{-4}$  Tesla

**0.31–0.58 gauss** – the Earth's magnetic field at its surface

**50 gauss** – a typical refrigerator magnet

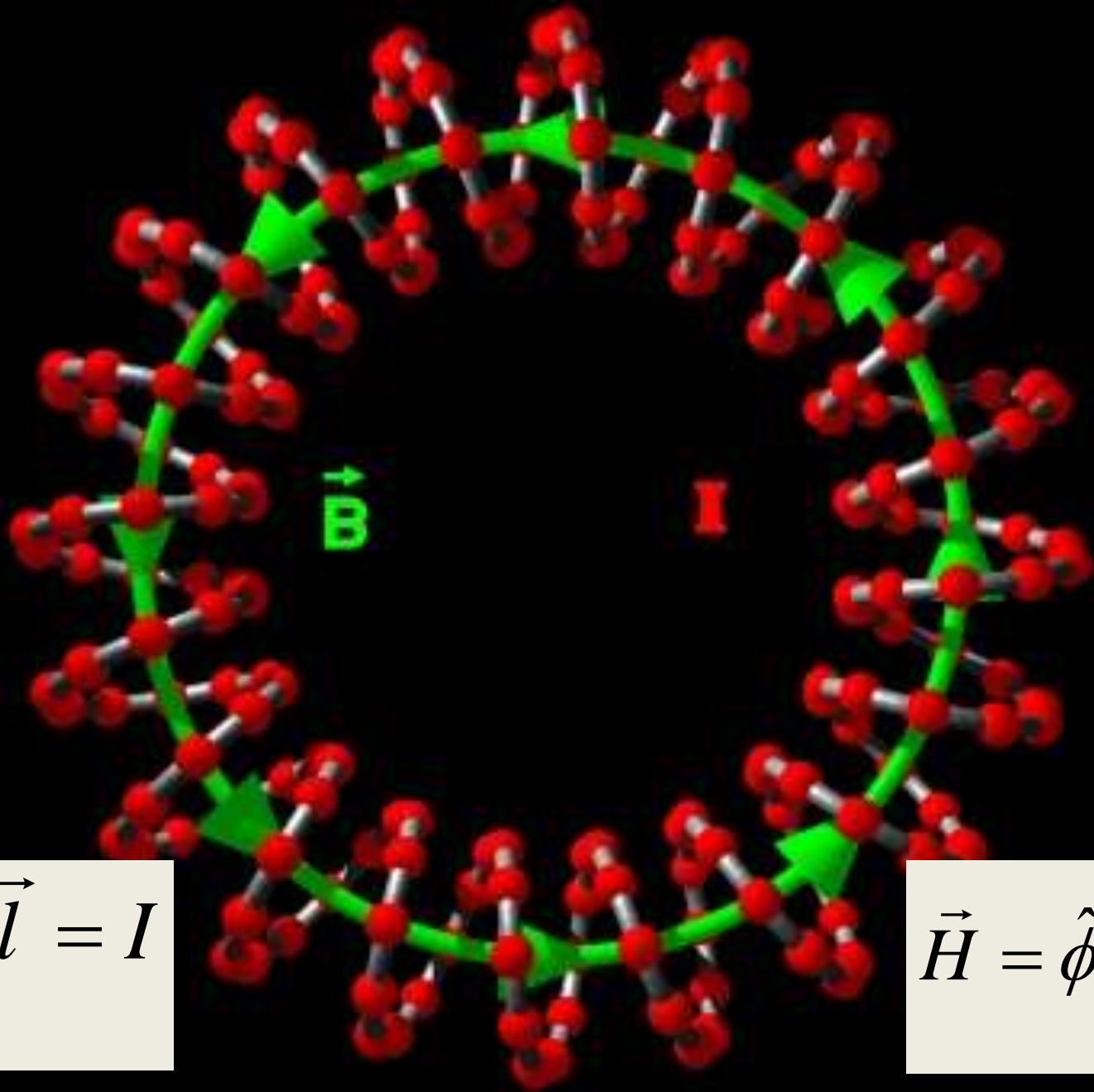
**2000 gauss** – a small neodymium-iron-boron (NIB) magnet



$$\vec{H} = \frac{I}{4\pi} \int_C \frac{d\vec{\ell} \times \hat{R}}{R^2}$$

this is the vector  
that points from  
the incremental  
Line element to the  
point where we're  
calculating  $\vec{H}$

this is NOT the spherical  
coordinate system  
unit vector.

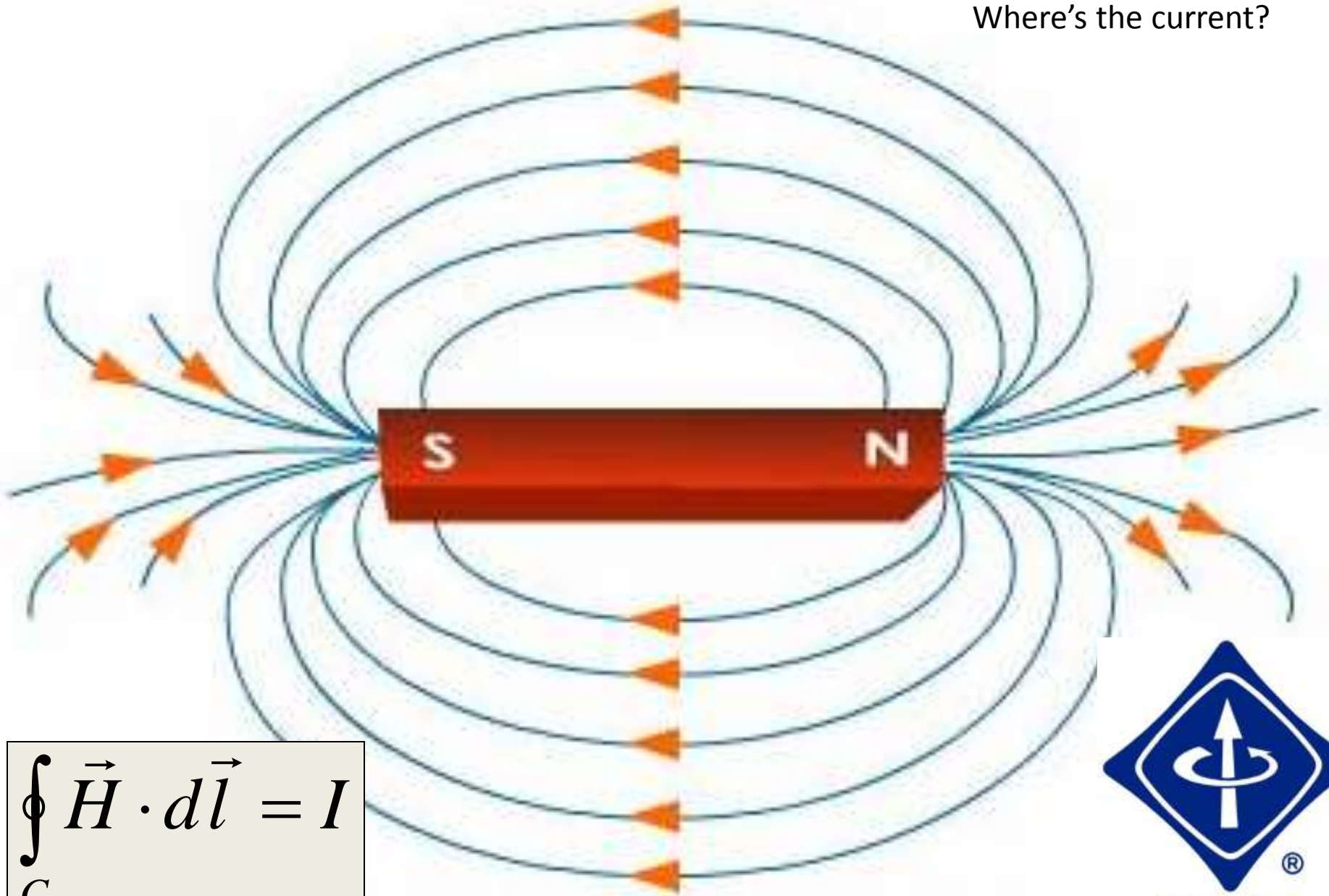


$$\oint_C \vec{H} \cdot d\vec{l} = I$$

$$\vec{H} = \hat{\phi} \frac{NI}{2\pi r}$$

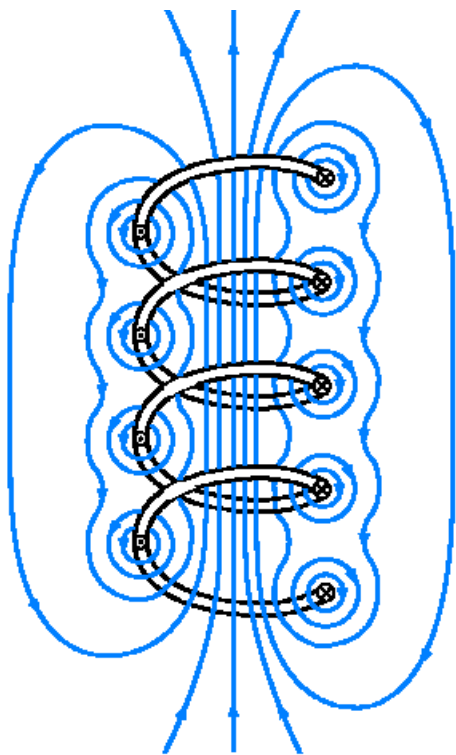


Where's the current?

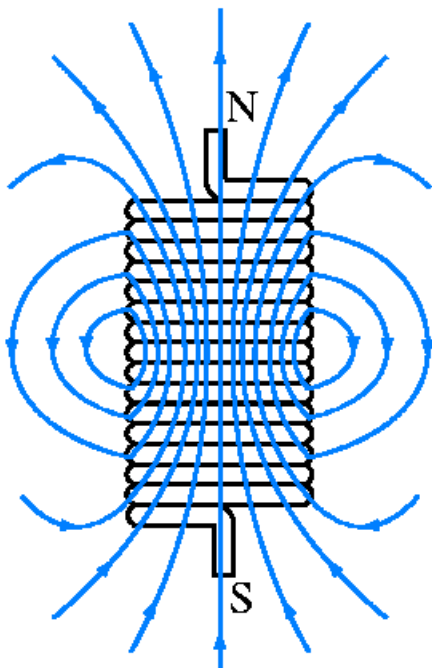


$$\oint_C \vec{H} \cdot d\vec{l} = I$$





(a) Loosely wound solenoid



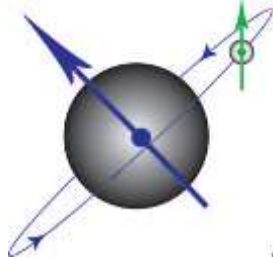
(b) Tightly wound solenoid

$$\mathbf{B} \simeq \hat{\mathbf{z}}\mu nI = \frac{\hat{\mathbf{z}}\mu NI}{l} \quad (\text{long solenoid with } l/a \gg 1)$$



Why so loose??... don't the gaps in the windings let the magnetic field out??

**Magnetic permeability,  $\mu$  [H/m]**  
 (related to the magnetization properties of the materials)



$$\vec{M} = \chi_m \vec{H}$$

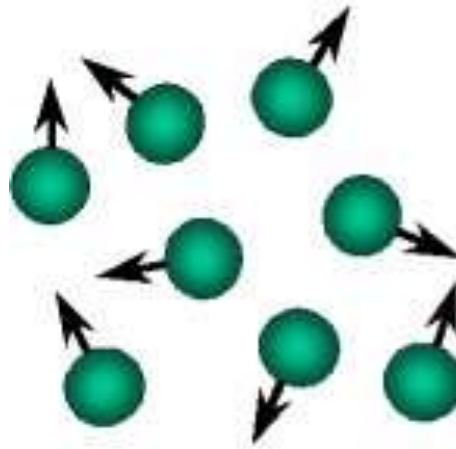
$$\vec{B} = \mu_0 (\vec{H} + \vec{M}) = \mu_0 (1 + \chi_m) \vec{H} =$$

$$\mu = \mu_r \mu_0$$

$\mu_r \cong 1 (< 1)$  – diamagnetic

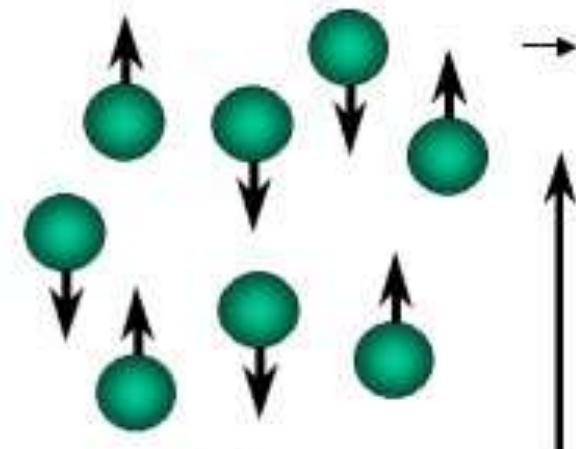
$\mu_r \cong 1 (> 1)$  – paramagnetic

$\mu_r \gg 1$  – ferromagnetic



$$\vec{B}_0 = 0$$

Randomly oriented

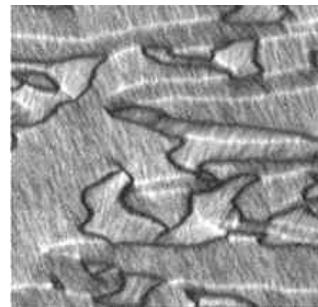


$$\vec{B}_0 > 0$$

Highly oriented



Each nucleus behaves like a bar magnet.



Electrons in an atom, or

*Domain walls in a soft magnetic sputtered FeN (50 nm) / Al<sub>2</sub>O<sub>3</sub> (5 nm) / FeN (50 nm) film structure*

# MATERIALS

$$\vec{H} \equiv \frac{1}{\mu_0} \vec{B} - \vec{M}$$

magnetization vector

$$\Rightarrow \vec{B} = \mu \vec{H}$$

for Linear Materials

$$\mu = \mu_r \mu_0$$

$$\mu_r \sim 10^5 \text{ for iron}$$

Thus,  $\mu_r \simeq 1$  or  $\mu \simeq \mu_0$  for diamagnetic and paramagnetic substances, which include dielectric materials and most metals. In contrast,  $|\mu_r| \gg 1$  for ferromagnetic materials;  $|\mu_r|$  of purified iron, for example, is on the order of  $2 \times 10^5$ .

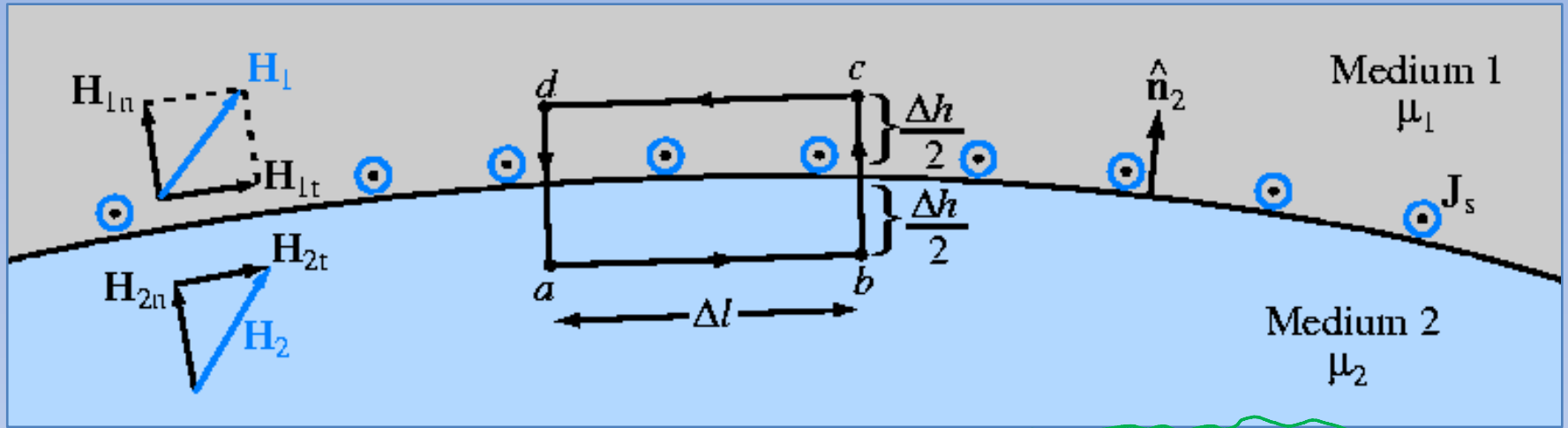
	Diamagnetism	Paramagnetism	Ferromagnetism
Permanent magnetic dipole moment	No	Yes, but weak	Yes, and strong
Primary magnetization mechanism	Electron orbital magnetic moment	Electron spin magnetic moment	Magnetized domains
Direction of induced magnetic field (relative to external field)	Opposite	Same	Hysteresis [see Fig. 5-22]
Common substances	Bismuth, copper, diamond, gold, lead, mercury, silver, silicon	Aluminum, calcium, chromium, magnesium, niobium, platinum, tungsten	Iron, nickel, cobalt
Typical value of $\chi_m$	$\approx -10^{-5}$	$\approx 10^{-5}$	$ \chi_m  \gg 1$ and hysteretic
Typical value of $\mu_r$	$\approx 1$	$\approx 1$	$ \mu_r  \gg 1$ and hysteretic

$\sigma = ?$   $\vec{B} = \mu \vec{H}$

when is  $\mu_r$  not one??



# Boundaries

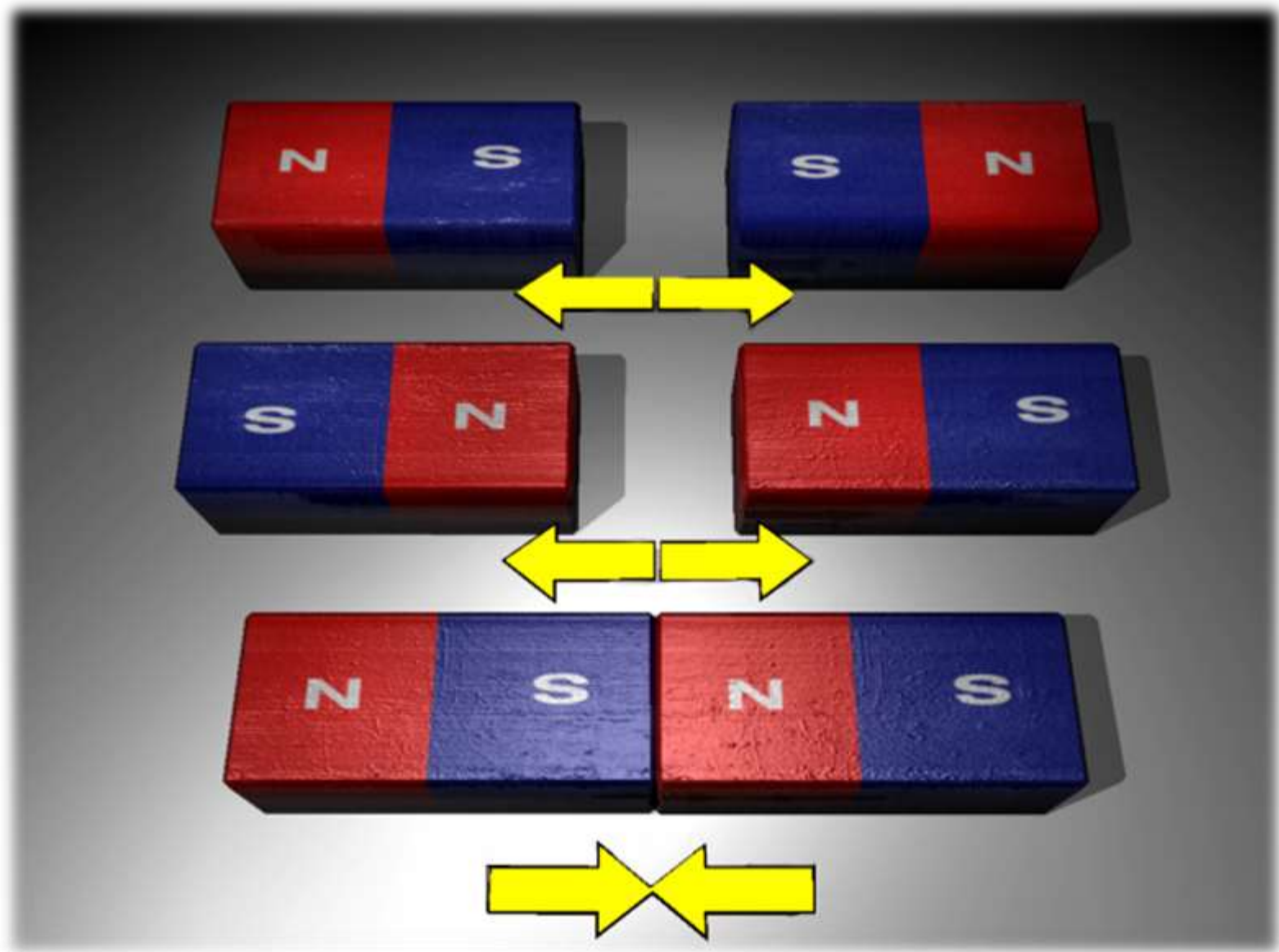


$$\oint_S \vec{B} \cdot d\vec{s} = 0 \Rightarrow B_{1n} = B_{2n}$$

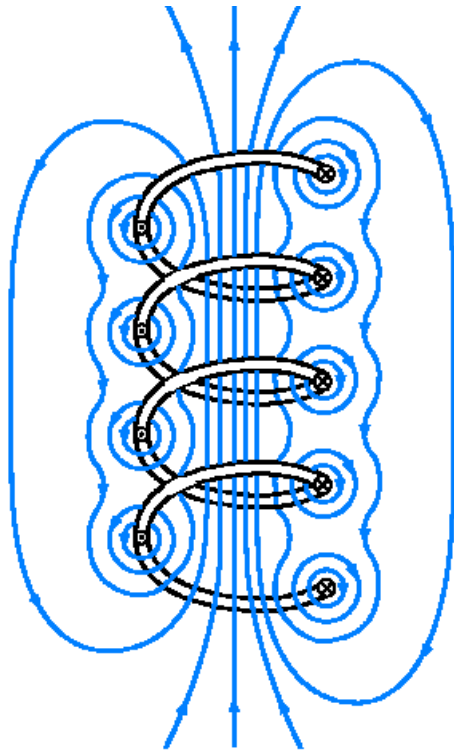
$$\oint_C \vec{H} \cdot d\vec{l} = I \Rightarrow \hat{n}_2 \times (\vec{H}_1 - \vec{H}_2) = \vec{J}$$

$$\text{If } \vec{J}_s = 0,$$

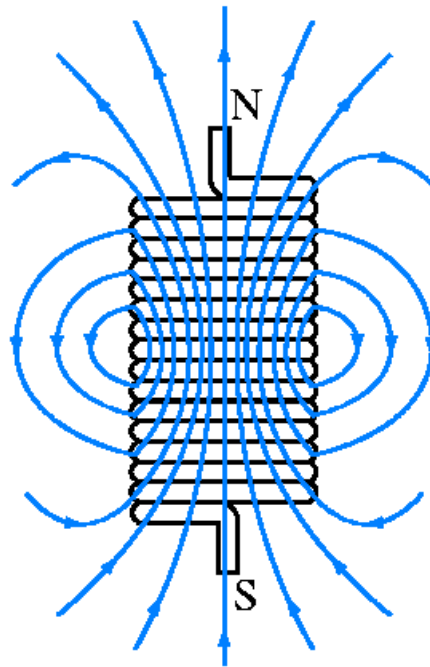
$$H_{1t} = H_{2t}$$



# Inductors



(a) Loosely wound solenoid



(b) Tightly wound solenoid

**Why Coilcraft wirewound chip inductors are your #1 choice**



**Higher Q** Compared to non-wirewounds, our chip inductors usually have Qs that are 50 to 100% higher.

**Lower DCR** For up to 3 times more current through our chip inductors thanks to their low DCR resistance.

**Higher SRF** The solenoid winding of our inductors gives them a much higher SRF than multilayer parts.

**Tighter tolerance** Precision manufacturing lets us consistently make parts with  $\pm 2\%$  inductance tolerance. Many popular values also come in  $\pm 1\%$ .

**Better support** With our engineers friendly web site, interactive design tools and generous free samples, Coilcraft is not just a company to do business with. Visit [www.coilcraft.com](http://www.coilcraft.com) for information on all our high performance wirewound inductors.



[www.coilcraft.com](http://www.coilcraft.com)

**Inductance**

\* self

\* mutual

units of  $\text{Wb/A} = \text{H}$   
(henries)

# Inductance

$$L = \mu \frac{N^2}{l} S \quad (\text{solenoid}), \quad (5.95)$$

and for two-conductor configurations similar to those of Fig. 5-27,

## Magnetic Flux

$$\Phi = \int_S \mathbf{B} \cdot d\mathbf{s} \quad (\text{Wb}).$$

## Flux Linkage

$$\Lambda = N\Phi = \mu \frac{N^2}{l} IS \quad (\text{Wb})$$

## Inductance

$$L = \frac{\Lambda}{I} \quad (\text{H}).$$

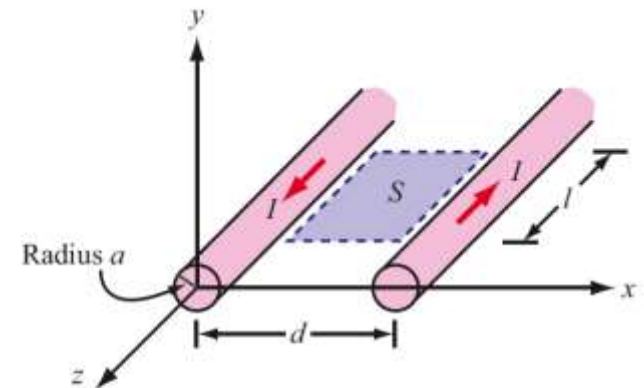
## Solenoid

$$L = \mu \frac{N^2}{l} S \quad (\text{solenoid}), \quad (5.95)$$

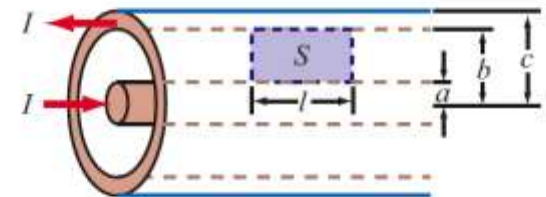
and for two-conductor configurations similar to those of Fig. 5-27,

$$L = \frac{\Lambda}{I} = \frac{\Phi}{I} = \frac{1}{I} \int_S \mathbf{B} \cdot d\mathbf{s}. \quad (5.96)$$

$$L = \frac{\Lambda}{I} = \frac{\Phi}{I} = \frac{1}{I} \int_S \mathbf{B} \cdot d\mathbf{s}. \quad (5.96)$$



(a) Parallel-wire transmission line



(b) Coaxial transmission line

**Figure 5-27:** To compute the inductance per unit length of a two-conductor transmission line, we need to determine the magnetic flux through the area  $S$  between the conductors.



# Example 5-7: Inductance of Coaxial Cable

The magnetic field in the region  $S$  between the two conductors is approximately

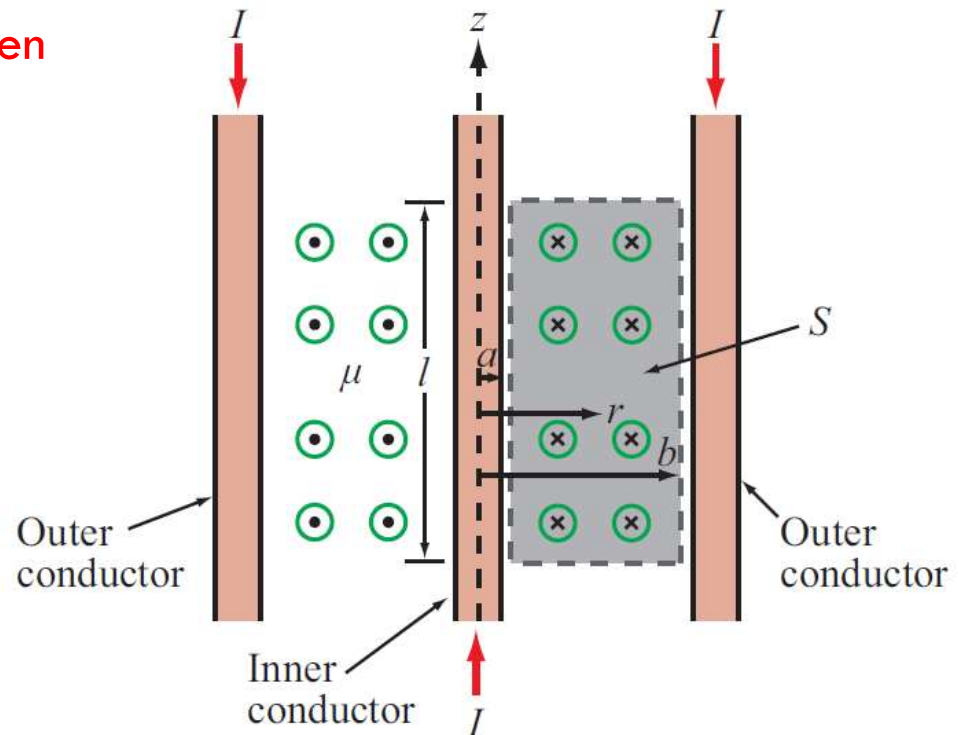
$$\mathbf{B} = \hat{\phi} \frac{\mu I}{2\pi r}$$

Total magnetic flux through  $S$ :

$$\Phi = l \int_a^b B \, dr = l \int_a^b \frac{\mu I}{2\pi r} \, dr = \frac{\mu I l}{2\pi} \ln \left( \frac{b}{a} \right)$$

Inductance per unit length:

$$L' = \frac{L}{l} = \frac{\Phi}{lI} = \frac{\mu}{2\pi} \ln \left( \frac{b}{a} \right).$$



**Figure 5-28:** Cross-sectional view of coaxial transmission line (Example 5-7).

# Magnetic Energy Density

$$w_m = \frac{W_m}{V} = \frac{1}{2} \mu H^2 \quad (\text{J/m}^3).$$

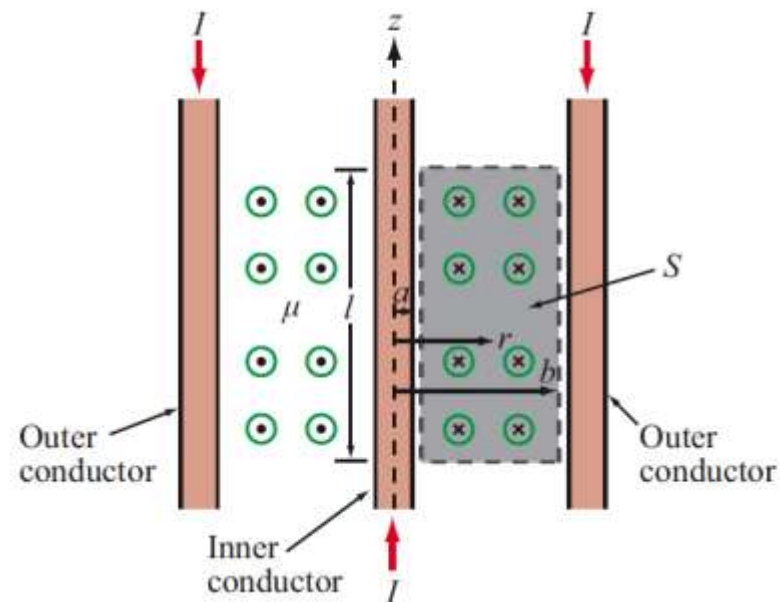
## Example 5-8: Magnetic Energy in a Coaxial Cable

Magnetic field in the insulating material is

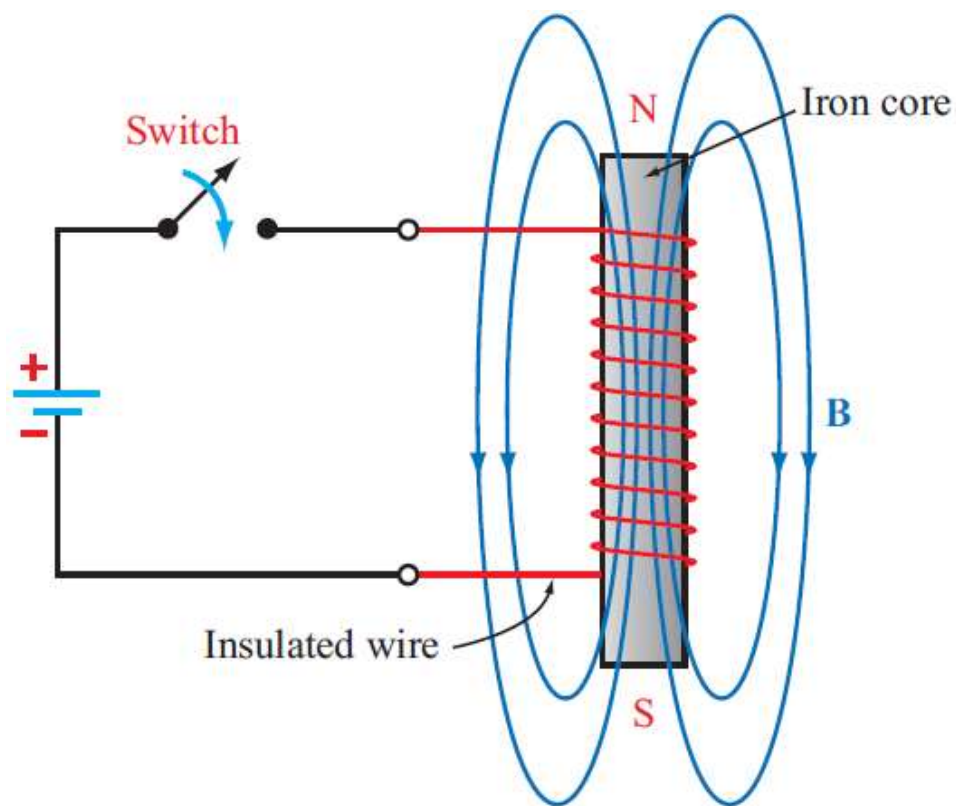
$$H = \frac{B}{\mu} = \frac{I}{2\pi r}$$

The magnetic energy stored in the coaxial cable is

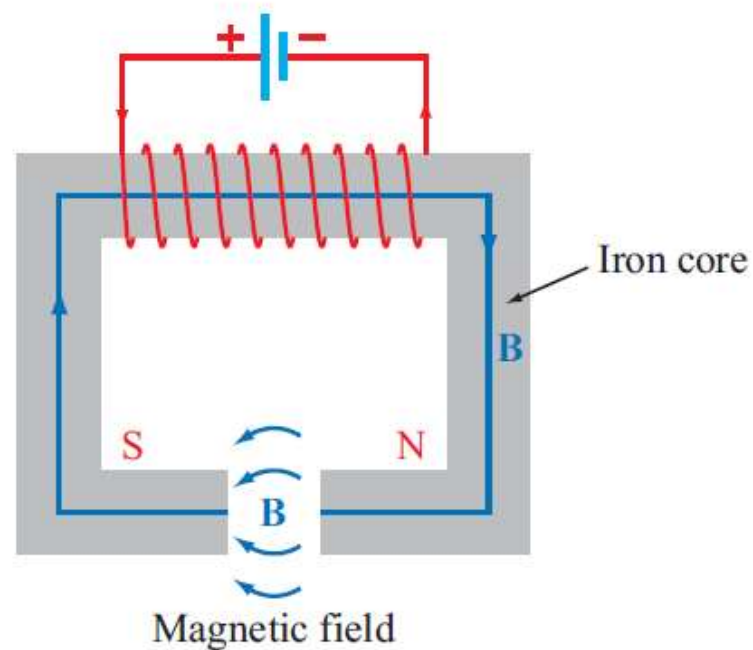
$$W_m = \frac{1}{2} \int_V \mu H^2 dV = \frac{\mu I^2}{8\pi^2} \int_V \frac{1}{r^2} dV$$



$$\begin{aligned} W_m &= \frac{\mu I^2}{8\pi^2} \int_a^b \frac{1}{r^2} \cdot 2\pi r l dr \\ &= \frac{\mu I^2 l}{4\pi} \ln \left( \frac{b}{a} \right) \\ &= \frac{1}{2} L I^2 \quad (\text{J}), \end{aligned}$$



(a) Solenoid



(b) Horseshoe electromagnet

**Figure TF10-1:** Solenoid and horseshoe magnets.

# Magnetic Energy Density

## Example 5-8: Magnetic Energy in a Coaxial Cable

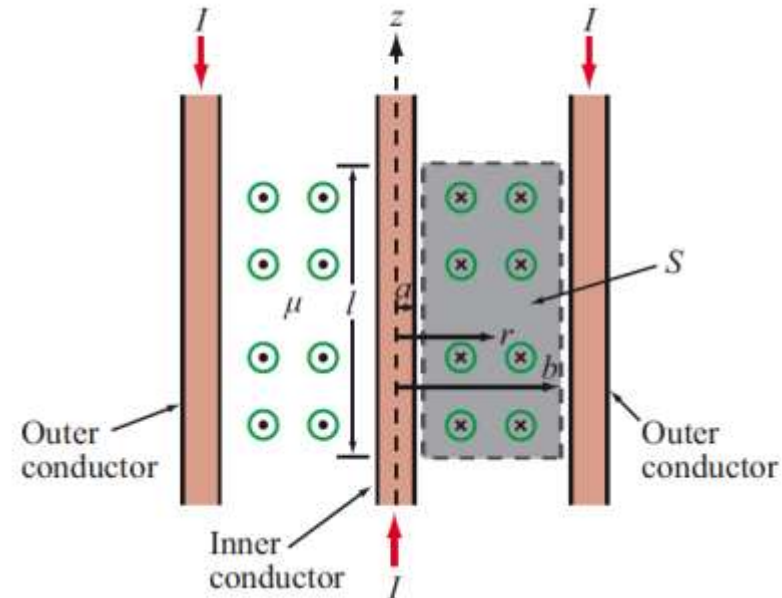
Magnetic field in the insulating material is

$$H = \frac{B}{\mu} = \frac{I}{2\pi r}$$

The magnetic energy stored in the coaxial cable is

$$W_m = \frac{1}{2} \int_V \mu H^2 dV = \frac{\mu I^2}{8\pi^2} \int_V \frac{1}{r^2} dV$$

$$w_m = \frac{W_m}{V} = \frac{1}{2} \mu H^2 \quad (\text{J/m}^3).$$



$$\begin{aligned} W_m &= \frac{\mu I^2}{8\pi^2} \int_a^b \frac{1}{r^2} \cdot 2\pi r l dr \\ &= \frac{\mu I^2 l}{4\pi} \ln\left(\frac{b}{a}\right) \\ &= \frac{1}{2} L I^2 \quad (\text{J}), \end{aligned}$$

**Table 5-1:** Attributes of electrostatics and magnetostatics.

Attribute	Electrostatics	Magnetostatics
<b>Sources</b>	Stationary charges $\rho_v$	Steady currents $\mathbf{J}$
<b>Fields and Fluxes</b>	$\mathbf{E}$ and $\mathbf{D}$	$\mathbf{H}$ and $\mathbf{B}$
<b>Constitutive parameter(s)</b>	$\varepsilon$ and $\sigma$	$\mu$
<b>Governing equations</b>		
• <b>Differential form</b>	$\nabla \cdot \mathbf{D} = \rho_v$ $\nabla \times \mathbf{E} = 0$	$\nabla \cdot \mathbf{B} = 0$ $\nabla \times \mathbf{H} = \mathbf{J}$
• <b>Integral form</b>	$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$ $\oint_C \mathbf{E} \cdot d\mathbf{l} = 0$	$\oint_S \mathbf{B} \cdot d\mathbf{s} = 0$ $\oint_C \mathbf{H} \cdot d\mathbf{l} = I$
<b>Potential</b>	Scalar $V$ , with $\mathbf{E} = -\nabla V$	Vector $\mathbf{A}$ , with $\mathbf{B} = \nabla \times \mathbf{A}$
<b>Energy density</b>	$w_e = \frac{1}{2} \varepsilon E^2$	$w_m = \frac{1}{2} \mu H^2$
<b>Force on charge <math>q</math></b>	$\mathbf{F}_e = q\mathbf{E}$	$\mathbf{F}_m = q\mathbf{u} \times \mathbf{B}$
<b>Circuit element(s)</b>	$C$ and $R$	$L$



